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CENTRIFUGALLY-SPUN CERAMIC/CARBON COMPOSITE FIBERS AND THEIR USE
AS ANODE MATERIALS IN LI-ION BATTERIES

A Thesis

by

GABRIEL GONZALEZ

Submitted to the Graduate College of
The University of Texas Rio Grande Valley
In partial fulfillment of the requirements for the degree of

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May 2021

Major Subject: Mechanical Engineering

CENTRIFUGALLY-SPUN CERAMIC/CARBON COMPOSITE FIBERS AND THEIR USE
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GABRIEL GONZALEZ

COMMITTEE MEMBERS

Dr. Mataz Alcoutlabi
Chair of Committee

Dr. Horacio Vasquez
Committee Member

Dr. Javier Ortega
Committee Member

May 2021

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ABSTRACT

Gonzalez, Gabriel, Centrifugally-Spun Ceramic/Carbon Composite Fibers and their use as Anode Materials in Li-Ion Batteries. Master of Science Engineering (MSE), May, 2021, 66 pp, 1 table, 34 figures, references, 97 titles.

The work in this thesis focuses on the processing of ceramic/carbon composite fibers via centrifugal spinning for use as anode materials in lithium-ion batteries (LIBs). Due to their high theoretical capacity, abundance, and environmental friendliness, metal oxides have been widely studied as alternate anode materials for lithium-ion batteries. In this research work, we report the synthesis of $\text{SnO}_2\text{:TiO}_2$ / flexible and porous carbon composites ($\text{SnO}_2\text{:TiO}_2\text{/FPCFs}$) . When applied as a binder free anode, the (3:2) $\text{SnO}_2\text{:TiO}_2\text{/FPCFs}$ demonstrated a high theoretical capacity of 900 mAh g^{-1} after 100 cycles at a current density of 100 mA g^{-1} . Furthermore, the as prepared ceramic/carbon composite fibers also demonstrated good cycling reversibility after testing at different current rates. For comparison, the results of pure ceramic composites as well as pure FPCFs are also provided.

DEDICATION

The completion of my master's studies would have not been possible without God, my family, friends, and educators. "Claim to me and I will answer you and tell you great and unsearchable things you do not know". With this biblical verse I want to first thank God for his blessings throughout my personal life and career.

To my mother, Veronica Torres, thank you for your unconditional love, for always providing for me and my sisters, and for teaching me to always maintain a positive attitude towards any circumstance. I will forever be grateful to God for blessing me with such a strong mother, I love you. To my father, Juan Gabriel Gonzalez, thank you for inspiring me to always believe in myself, have good work ethic, and remain humble.

To my grandparents: Francisco Torres, Maria Santa Ramirez, Jesus Gonzalez, Julia Hernandez, thank you all so much for the shared memories, unconditional love, advice, and support. I have much love for all of you and I promise to always keep working hard to represent your teachings and hard work wherever I go.

Finally, to my younger sisters Alondra, and Alejandra, to show you girls that anything is possible with hard work, dedication, and faith.

ACKNOWLEDGMENTS

I want to thank my committee chair, Dr. Mataz Alcoutlabi for pushing me beyond my limits and showing me that I can do great things. I would also like to thank Dr. Horacio Vasquez and Dr. Javier Ortega for their advice during my undergraduate and graduate studies. Also, thank you to Dr. Karen Lozano for giving me an opportunity to be part of the PREM and for inspiring many students to not be limited by their background.

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CHAPTER I

INTRODUCTION

The high demand for energy has led to excessive use of fossil fuels which resulted in many environmental issues that are accompanied by a large CO₂ emission. Lithium-ion batteries (LIBs) are considered as an alternative energy source to fossil fuel for use in electric vehicles (EVs), electronics and portable devices due to their compact size, high energy density, and high specific lithium storage capacity, [1-3]. Although they have proved outperform other sources of power such as wind and solar energy, LIBs have not yet reached their optimal potential. Currently, the most common anode material used in LIBs is graphite, but it can only deliver a specific capacity of 372 mAh g⁻¹ [4-6]. Another limiting factor of graphite is the formation of dendrites on its surface during rapid charging. Such phenomenon leads to low Li-ion diffusivity that can deteriorate the electrochemical performance of the battery[7-9].

Current advancements in nanotechnology have enabled the manufacturing of new nano composites with unique microstructures and morphologies. Due to their distinct characteristics and high surface area, nanocomposites have demonstrated improved performance in a wide variety of applications compared to their bulk counterpart[10-12]. For example, porous, hollow, and tubular are features of the different structures that have been achieved through nanocomposite production methods, which include centrifugal spinning, melt blowing, and electrospinning [13-15].Such morphologies increase the surface area per unit volume of the

material and provide numerous active sites that allow more lithium interaction within the anode during the charge/discharge process. As a result, larger specific capacities and higher energy densities that surpass those of graphite can be obtained. [5, 10]. In the search for alternate anode materials, metals such as Sn, Ti, Fe as well as their respective oxides have been widely investigated as alternate anode materials in LIBs due to their distinct chemical and physical characteristics that can result in high capacities ranging from 500-1000 mAh g⁻¹ [16-19]. More recently, nano/micro structured metal oxides have been synthesized through various methods for use as alternate anode materials for LIBs and have exhibited better electrochemical performance when compared to their bulk counterpart. In addition, metal oxides are of interest due to their environmental friendliness, abundance, and low cost[20, 21]. Sn and SnO₂ have been widely investigated as an alternate anode material due to their high theoretical capacity of 993.4 mAh g⁻¹ and ~782 mAh g⁻¹ respectively [22-25]. Despite its high capacity, Sn suffers from a high volume expansion during the alloying/dealloying process with lithium which can result in anode cracking and capacity fading [26-28]. Similarly, SnO₂ is brittle material and suffers from huge volume expansion after prolonged charge/discharge cycles leading to pulverization of the anode and poor cycling performance. To improve the electrochemical performance of Sn and SnO₂ anodes, the design of new nano/micro-structures and combination with other materials such as TiO₂ and carbon have been recently investigated [22-24, 27, 29-31]. TiO₂ has been of interest in LIB research for its excellent rate performance, low volume change upon cycling and good capacity retention over long periods of time. When combined with Sn and SnO₂, TiO₂ forms a unique heterojunction which is well known for its good kinetics and synergistic effect which can result in an improved anode performance [25, 32-37].

Although, Sn/TiO₂, and SnO₂/TiO₂ composites have shown promising results when compared to pure Sn and SnO₂, but they still suffer from pulverization after prolonged charge/discharge cycles. To further improve the electrochemical performance of Sn and SnO₂, various carbon coating methods have been explored to mitigate the large volume change and stresses during cycling [6, 19, 25, 28, 37-42]. Due to their high porosity and distinct structures, carbon fibers (CFs), have been widely used as stress buffer matrices for metal and metal oxide-based anodes. Compared to their bulk counterpart, CFs, provide larger numbers of reaction sites for Li-ion intercalation that can result in a high anode capacity[43-45].

Currently, electrospinning has been amongst the most used methods to process various composite carbon fibers such as porous, hollow, and multichannel structures and have significantly exhibited promising results when used as stress buffer matrices for metal-oxide anodes. Electrospinning is a process that allows facile fiber production and allows the synthesis of various metal oxide/carbon fibers with distinct nanostructures for LIB and many other applications[46-48]. For example, Haoyi Mou used electrospinning to prepare encapsulated SnO₂/TiO₂ particles into carbon nanofibers. Tianyu Li et al, synthesized porous carbon nanofibers containing Sn/Ti nanoparticles through electrospinning and subsequent heat treatment. When used as an anode material in LIBs, the Sn/Ti/C composite fibers delivered a capacity of 557 mAh g⁻¹ at 100 mA g⁻¹ which is higher than that of graphite. Additionally, the as-synthesized composite fibers demonstrated a capacity retention of 98.7 % after 100 cycles at a current density of 50 mA g⁻¹ which was attributed to the buffering effect of the flexible carbon-fiber matrix[40, 49-52]. Although good results have been reported using electrospinning, the required high applied voltage as well as long production rates, limit the use of this technology for the high production rate of fibers[48, 53].

More recently, centrifugal spinning has been explored as an alternate method to produce carbon fiber composites. As opposed to electrospinning, centrifugal spinning relies solely on centrifugal forces and high rotational speeds to yield large amounts of fibers [43, 53-55]. Currently, centrifugally spun composite fibers have been used as binder-free anodes in LIB and sodium-ion batteries (SIB) and have exhibited good electrochemical performance[56-58]. Agubra et al synthesized Sn/C composite fibers via centrifugal spinning of Sn/ poly(acrylonitrile) (PAN) precursor solutions followed by a subsequent heat treatment. When applied as a binder-free anode in Li-ion half cells, the Sn/C composite fibers delivered a high reversible capacity of 724 mAh g⁻¹ after 50 cycles at a current density of 100 mA g⁻¹ which was attributed to the flexible and amorphous structure of the CFs[59]. Work reported on Centrifugally spun SnO₂/C composite-fiber anode for SIBs showed that the composite anode delivered a capacity of 158 mAh g⁻¹ after 100 cycles at 640 mA g⁻¹ and exhibited good rate performance. Though improved electrochemical results have been obtained by centrifugal spinning, such technology still faces some challenges. For example, high loadings of active material (e.g. Sn, Si, Sb nanoparticles) in the precursor solution and uniform distribution of active material within the fibers can be difficult to achieve due to the high viscosity and particle agglomeration in the solution. Although solutions with high viscosity are preferred for centrifugal spinning, compared to electrospinning, the addition of active material to the polymer solution can largely increase the solution viscosity and can negatively affect the formation and the production rate of the composite fibers [56, 60, 61]. To address these issues, different coating methods have been explored to load the active material (e.g., nanoparticles or short fibers) onto centrifugally spun precursor fibers with the aim to improve the anode performance [62, 63].

In the present work, ternary $\text{SnO}_2\text{:TiO}_2\text{/FPCFs}$ composites were prepared by centrifugal spinning of precursor solutions and subsequent heat treatment. The characterization of the composite fibers was studied by SEM, TEM, XRD, XPS, and TGA. Moreover, when used as a binder-free anode in LIBs, the $\text{SnO}_2\text{:TiO}_2\text{/FPCFs}$ composite anode with (3:2) $\text{SnO}_2\text{:TiO}_2$ ratio demonstrated outstanding electrochemical results. For comparison, the electrochemical results of $\text{SnO}_2\text{/FPCFs}$ and $\text{SnO}_2\text{:TiO}_2\text{/FPCFs}$ with (1:1) $\text{SnO}_2\text{:TiO}_2$ ratio were also investigated.

CHAPTER II

LITERATURE REVIEW

2.1 The Lithium-ion Battery

The main components in a Lithium Ion Batteries (LIB) are the cathode, the anode, a separator, and a pair of current collectors [64].

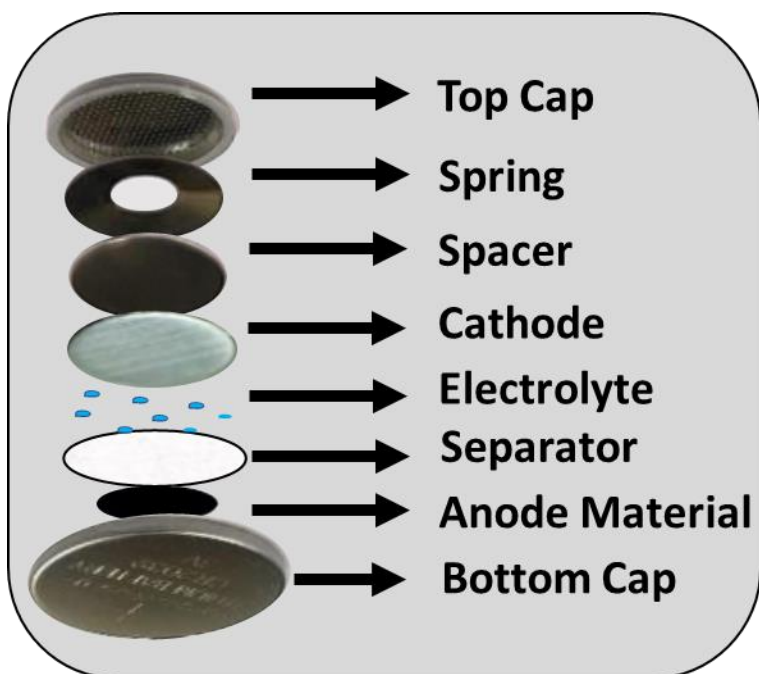


Figure 1. Schematic of a lithium ion battery coin cell

The cathode is the positive electrode and the main lithium source of a LIB. The most popular cathodes used in commercial LIBs are materials which have high positive redox potentials such as LiCoO_2 , LiMn_2O_4 , and LiFePO_4 . In the other hand, the anode is the negative electrode and is mainly responsible for dictating the amount of lithium a LIB can retain.

Currently, the most common anode material used in commercial LIB is graphite with theoretical reversible capacity of 372 mAhg^{-1} . Both electrodes are divided by an electrolyte filled separator. The separator is usually made from a fiber glass porous enough to allow the transfer of Li-ions between the cathode and the anode yet small enough to prevent the passage of electrons and direct contact between electrodes that can lead to a short circuit. Moreover, the current collectors serve as a conductive path for electrons to transfer from one side to the other and create a current that is supplied to any accessory being powered [16, 65]. The most common current collector material used on the cathode is aluminum due to its stability at high oxidation potentials. On the other hand, the most common current collector material used for the anode is copper due to its excellent stability at low oxidation potentials as well as thermal stability [64].

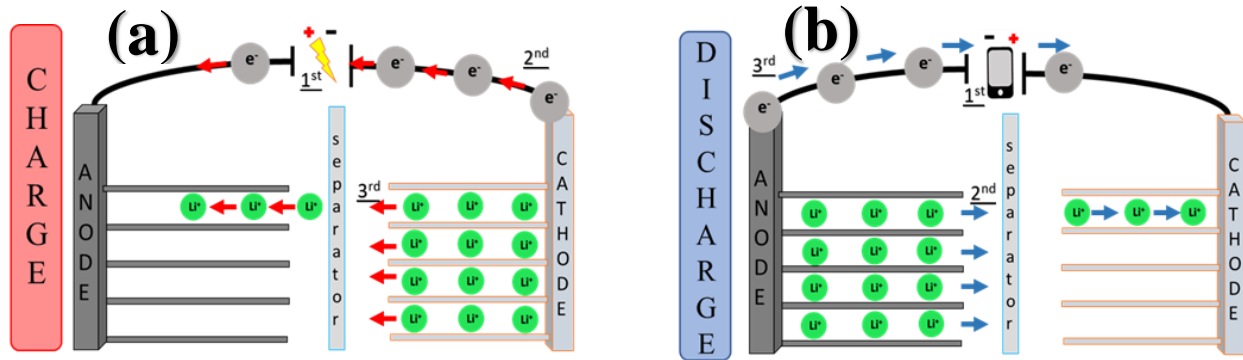


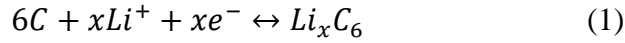
Figure 2. Working principle of a battery

2.1.1 The Principle of Operation in LIBs

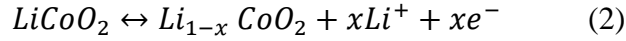
Figure 2 illustrates the process that takes place inside LIBs during the charge (a)/ and discharge (b) discharge cycling process. During the charge process the cathode releases Li Ions that travel through the separator and conductive electrolyte to intercalate into the anode. Vice versa, during the discharge process the Li ions return from the anode to the cathode and complete what is known to be one charge/discharge cycle. Equations 1 and 2 illustrate the two reversible

chemical reactions that occur in the anode and cathode upon charge/discharge cycling, respectively.

Anode:



Cathode:



When a full cell is being charged, a significant amount of electrons travel to the anode from the cathode through the current collectors resulting in a reduction and oxidation reaction at the anode and cathode respectively. These reactions are reversible and opposite of each other; therefore, during the discharge process the anode oxidizes while the cathode reduces. [4, 16].

2.2 The Anode Material

The anode material is the negative electrode, and it plays a major role when determining the overall lithium storage of a LIB. While charging/discharging a battery, the anode is responsible for the storage of Li ions and the release of these back into the cathode [4]. An anode electrode must be able to store large amounts of Lithium without pulverizing, form a stable solid-electrolyte interface (SEI) layer, be affordable, and environmentally friendly. Currently, the most common anode material used in commercial LIBs is graphitic carbon. Graphite can best be described as stack of hexagonal sheets of carbon bonded together by van der Waals forces. During the charge process Li ions are inserted in between graphite planes through an intercalation mechanism [16, 66]. Some of the advantages of graphite are its ability to form a controlled and stable SEI layer and its low volume change during insertion/desertion of Lithium while cycling. Although graphite has been an efficient anode material it limits the capacity

storage of LIBs. During lithium intercalation 6 carbon atoms are necessary to intercalate one Li ion. This results in a low theoretical reversible capacity of 372 mAhg^{-1} , a small power density, and poor transport rates which are usually less than $10^{-6} \text{ cm}^{-2} \text{ s}^{-1}$. To enhance the overall Li^+ storage an improved anode material that can interact with more Li anodes without pulverizing is required [16, 17, 65].

2.3 Alternate Anode Materials

Recent advancements in nanotechnology have paved the road for the synthesis of enhanced nanostructured anode materials. Currently, many nano- and micro- metal oxides and their composites have been widely investigated as alternate anode material in LIBs due to their high lithium capacity, environmental friendliness, and abundance. As opposed to their bulk volume material, nano structured materials have demonstrated different physical and chemical properties that result in an enhanced electrochemical performance. Their small size provides shorter lithium paths and allow a greater surface area to be exposed to the electrolyte. Although outstanding results have been observed in current literature, nanostructured materials still face several drawbacks; therefore, further work is needed in order to ensure safety, stability, and good electrochemical performance

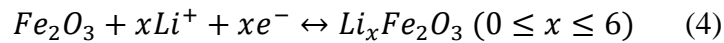
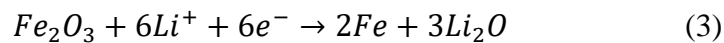
2.3.1 Metal Oxides

Synthesizing a material that demonstrates good stability upon cycling has been a major issue for rechargeable LIBs. New alternative electrode materials are needed to improve the efficiency and cyclability of LIBs over prolonged charge/discharge cycles and life shelf [17]. Metal oxides can interact with Li by alloying, insertion, and conversion reaction mechanisms. Metal oxides react with Li through a conversion reaction mechanism and are known to possess

rich and chemical properties that makes them good candidates for anode material. Although metal oxides suffer from low electrical conductivity, thick SEI layer formation, and volume change they can deliver high reversible capacities between 500-1000 mAhg⁻¹ [16]. Current advancements in nanotechnology have allowed the synthesis of nano structured metal oxides such as Fe₂O₃, SnO₂, and TiO₂ which have been widely studied as alternate anode material for LIBs due to their unique electrochemical characteristics at the nano level.

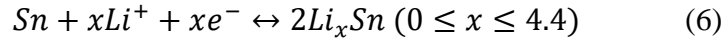
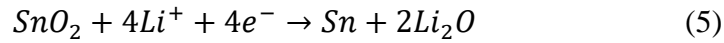
2.3.2 Iron Oxide based Anodes

Hematite Fe₂O₃ is a transition metal oxides that has been widely studied as anode material since it is due to its high theoretical capacity of 1007 mAhg⁻¹. Unlike carbon, one molecule of Fe₂O₃ has the capability of interacting with 6 lithium molecules instead of one. The overall reactions of Fe₂O₃ with lithium are presented in equations (3,4) [18, 67, 68]. Another characteristic that makes this material attractive is that it can be easily synthesized through different non-hazardous techniques such as hummers salts, sol-gels, and precipitation. Despite its good attributes, Fe₂O₃ is susceptible to large internal structural stresses that result in a large volume expansion and lead to poor electrochemical performance over prolonged charge/discharge cycling. Tubular, core shell, and hollow nanostructures are some examples of the different morphologies that have been widely proposed as solutions to mitigate the drawbacks experienced by Fe₂O₃. In addition, the creation of different Fe₂O₃/carbon composites has also been explored as a method to alleviate the internal stresses experienced by Fe₂O₃.



2.3.3 Tin Oxide Anodes

Another metal oxide that has gained much popularity due to its high theoretical capacity of 782 mAhg⁻¹ is tin dioxide (SnO₂). One major reaction that makes SnO₂ interesting is its irreversible reduction process of SnO₂ to metallic Sn as represented in equation 5 [35]. Such reaction contributes to the irreversible capacity loss during the first charge/discharge cycle; however, it also prevents further pulverization of the material and results in a reversible alloying/dealloying process between Sn and Li as shown in equation 6. This reaction is mainly responsible for the high theoretical capacity of SnO₂ which doubles that of graphite.

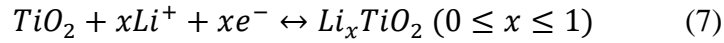


However, like most metal oxides, SnO₂ faces a large volume expansion and capacity decay upon cycling [35, 69]. This drawback leads to harmful mechanical strains and stresses that are responsible for the pulverization of the anode material and results in a poor electrochemical performance. In order to solve this issue several solutions have been proposed such as hybrid nanostructures, downsizing the particles, and the combination of SnO₂ with a material that is less active [41, 70]

2.3.4 Titanium Oxide Anodes

Due to their semiconductive, photolytic, and electrochemical characteristics, TiO₂ composites are amongst the most popular metal oxides that have been studied in the fields of energy storage, chemical sensing, as well as in biomedical applications[12, 71]. Furthermore, their low cost, abundance, and environmental friendliness are also properties of TiO₂ nanocomposites to be considered for numerous battery and gas sensing applications [34, 36, 72,

73]. More recently, TiO_2 has been widely used in LIB application due to its great rate capabilities and cyclic stability upon cycling. When combined with other materials such as Sn, SnO_2 , and Fe, TiO_2 is known to mitigate the tremendous volume expansion; however, if used in excess it can hinder the overall capacity of the synthesized composite due to its low theoretical capacity of 323 mAh g^{-1} . The interaction of TiO_2 and lithium can be chemically represented by the following equation.



2.4 Centrifugal Spinning

Centrifugal spinning is a new method that has been gaining popularity in the area of nano/micro fiber processing and formation [44, 57, 74]. Unlike electrospinning, centrifugal spinning does not depend on high voltage and electric field to produce nano and micro composite fibers. Instead, centrifugal spinning depends solely on centrifugal forces caused by the spinneret rotational speed to produce nano and microfibers with high yield and in a short period of time [43, 75, 76]. However, high loadings and uniform distribution of active material within the fibers can be difficult to achieve due to the high viscosities and particle agglomeration when preparing solutions and during the spinning process, respectively. Although viscous solutions are preferred for this process, the addition of nanoparticles can largely increase the viscosity of a solution and impact the fiber production feasibility as well as the production rate. To resolve these issues, different coating methods have been explored to load nanoparticles onto centrifugally spun fibers and increase their electrochemical performance when used as anode material for LIBS.

CHAPTER III

EXPERIMENTAL PRODEDURES

3.1 State of the art equipment

The investigation to design an improved flexible binder free metal oxide microfiber anode will require the use of the following state of the art software and hardware equipment.



Figure 3. Cyclone Machine

The cyclone machine is a new technology owned by The University of Texas Rio Grande Valley. It is a machine that uses angular velocity and centrifugal forces to produce microfibers. This machine will be used to produce polymer precursor metal oxide microfibers. The varying parameters are the humidity and temperature of the room while the controllable parameters are the speed and time per cycle.



Figure 4. Vacuum Oven

The Vacuum Oven in Figure 4 will be used to store and dry under vacuum the obtained microfibers overnight. This is a crucial step in the overall process since it assures the evaporation of any leftover solvents and prevents any moisture from damaging the fibers.



Figure 5. OTF-1200X Furnace

The furnace illustrated in Fig 5 will be used to oxidize the obtained precursor metal oxide microfibers and to also carbonize them under an argon environment. The equipment is attached to an argon tank with a flowmeter and regulator that are used to control the amount of argon flowing through the tube. The obtained carbonized fibers are then cut into circular $\frac{1}{2}$ inch diameter anodes and assembled into coin cells to perform an electrochemical study.



Figure 6. MBraun Lab star pro glove box

Figure 6 shows the Mbraun Lab star pro glove box under argon environment which will be to assemble the obtained carbonized metal oxide microfiber anodes into lithium ion battery half cells.



Figure 7. Scanning Electron Microscope (SEM) and Energy Dispersive X-ray Analysis (EDAX)

The SEM instrument will be used to characterize the structure and surface morphology of the obtained polymer precursor and carbonized metal oxide microfibers. It is important to note that this SEM instrument is equipped with an Energy Dispersive X-ray Analysis (EDAX) instrument that will be used to determine the elemental composition of the metal oxide composite microfibers.



Figure 8. TG 209 Tarsus (TGA) Instrument

The TG 209 Tarsus is a thermogravimetric analysis (TGA) instrument that will be used to confirm the amount of metal oxide material within the obtained microfiber.



Figure 9. BioLogic Cyclic Voltammetry (CV) Instrumentation

The CV instrumentation will be used to study the oxidation/reduction reactions that will be happening in the metal oxide composite anode. This machine will be operated with a scan rate of 0.2 mV/s between 0 and 3 V at a frequency of 0.1 Hz and 1kHz respectively. The instrument will be connected to a computer equipped with BTLab which will be used to configure and observe the ongoing experiments.



Figure 10. Autolab 128 N Electrochemical Impedance Spectroscopy

The Autolab 128 N Electrochemical Impedance Spectroscopy will be utilized to study the electrolyte and interfacial resistance for comparison of cycled and uncycled cells. This instrument will be connected to a computer equipped with eh Nova 1.10 software which will serve to set up, run, and display experiments.



Figure 11. LANHE Battery Testing System

The LANHE Battery Testing System illustrated in figure 11 will be used to study the charge/discharge performance, columbic efficiency, and cyclic stability of the metal oxide composite microfiber anodes at different current densities over a charge/ discharge voltage of 3V and 0.05 V respectively. This machine will be connected to computer with a monitor equipped with LAND Battery Testing Monitor system software which will be used to set up and display the ongoing experiment.



Figure 12. Arbin Battery Testing System

Figure 12 displays the Arbin Battery Testing System which will be used to further analyze the performance and stability of the metal oxide composite anodes at different current rates set according to the anode's weight. The instrument will be connected to a computer and monitor that will be used to configure the desired settings of the experiment as well as to display and import results.

3.2 Fabrication of fiber composites

For the processing of the short fibers, Absolute ethanol (200 proof), Polyvinylpyrrolidone (PVP) with average molecular weight (MW) of 1,300,000 (99.5%), Tin II 2ethylhexanate (92.5-100%), Titanium IV butoxide (97%), Polyacrylonitrile with average Mw of 150,000, N, N-Dimethyl Formamide (DMF), SuperP carbon black and Poly methyl methacrylate (PMMA) were all purchased from Sigma-Aldrich and used without further modification.

3.2.1 Ceramic composite fibers anode preparation

Short metal-oxide microfibers were synthesized through the calcination of centrifugally spun precursor fibers. Briefly, 3 g of PVP were dissolved in 17 g of ethanol and the solution was stirred for 12 h at room temperature. Subsequently, 1.5 g of Tin(II) 2 ethylhexanate was added to the solution and the mixture was stirred for an additional 12 h to obtain a homogeneous solution. The solution was centrifugally spun at 9000 RPM with a relative humidity of 55% to prepare the precursor fibers. The pristine precursor fibers were heated in air at 700 °C for 3 h with a heating rate of 2 °C /min to yield SnO₂ short fibers. To obtain pure TiO₂ precursor fibers, the same process was used. Initially, 1.5 g of Titanium (IV) butoxide was added to prepare the precursor solution. The process was used to obtain the SnO₂/TiO₂ composite precursor solutions which were labeled as SnO₂/TiO₂ (3:2) and SnO₂/TiO₂ (1:1). To prepare anodes from the pure ceramic fibers first, the as prepared SnO₂/TiO₂ nanocomposites, with a ratio of 3:2, were crushed in a mortar and pestle, then 80 % of the short fibers, 10 % PAN, and 10 % carbon black were mixed in 1g of DMF to prepare a slurry. To obtain homogeneity, the as-prepared slurry was sonicated for 30 minutes and subsequently stirred for 12 hours. Subsequent to homogenization, the slurry was coated onto a copper foil and dried under vacuum at 60 °C for 24 hours. Once dry the coated slurry was heat treated in an argon filled tube furnace at 450 °C for 5 hours with a heating rate of

2 °C/min. After heating 0.5” circles were cut to be tested as an anode material. The processing method of the short metal oxide micro-fibers is shown in Figure 13 and the anode preparation is illustrated in Figure 14.

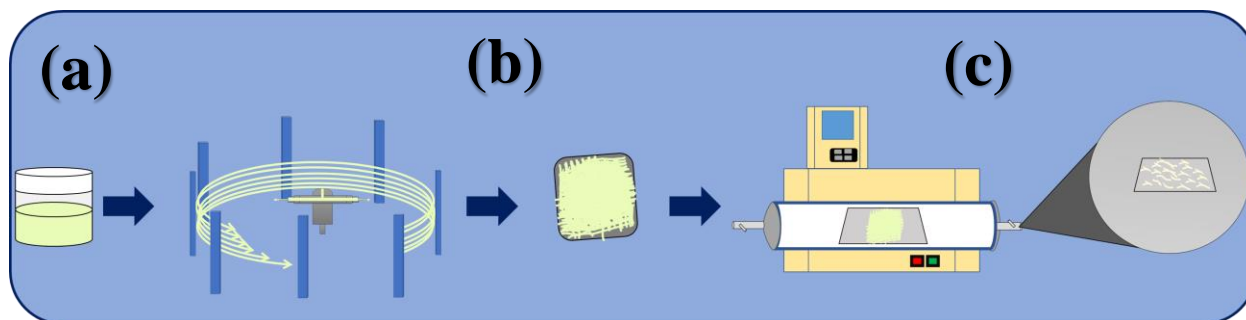


Figure 13. A schematic representation of metal-oxides fiber fabrication process: (a) polymer solution with metal-oxide precursors, (b) centrifugal spinning, and (c) calcination.

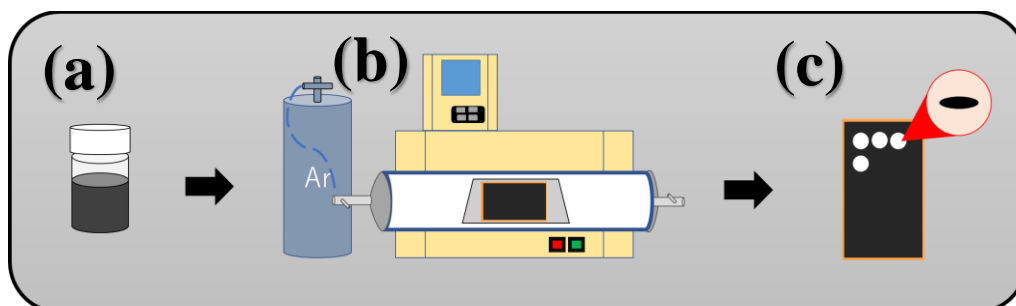


Figure 14. Schematic representation of short fibers slurry(a) heat treated at 450 C in argon (b) and (c) anode preparation.

3.2.2 Ceramic/carbon composite fibers anode preparation

1.92 g of PAN were dissolved in 17.6 g of DMF by magnetically stirring for 12 h to prepare a homogeneous solution. Then, 0.48 g of PMMA was added while the solution was left to stir for an additional 12 h at 60 °C. The PAN/PMMA solution was then loaded into a 3 mL syringe and fed into a spinneret to prepare centrifugally spun PAN/PMMA pristine fibers at 8500-9000 RPM with a relative room humidity of 55-60 %. The obtained precursor fibers were then dried under vacuum overnight at 60 °C to evaporate any remaining solvent. Prior to preparing the coating solution, TGA was conducted on the PAN/PMMA fibers to determine the amount of carbon yield after carbonization at 700 °C [77]. The coating solution was then prepared by mixing 50 wt% of short micro-belt fibers, with (3:2) ($\text{SnO}_2/\text{TiO}_2$) ratio in ethanol followed by sonication (1 h) and magnetic stirring for 24 h. The coating solution was then loaded into a 3ML syringe and was manually coated onto the pristine PAN/PMMA fibers. The coated fibers were then dried under vacuum at 60 °C for 24 h to evaporate any remaining solvent. To obtain flexible ternary $\text{SnO}_2/\text{TiO}_2/\text{C}$ composite fibers, the metal oxide coated precursor fibers were stabilized in air at 280 °C for 6 h (heating rate of 3 °C/min) and carbonized at 700 °C for 3 h in an argon filled tube furnace (heating rate of 5 °C/min). To prepare pure FPCFs, the same heat treatment was applied to PAN/PMMA pristine fibers. The obtained carbon fibers were cut into 0.5- discs and used as binder-free anodes in LIBs. This process can be represented by figure 15.

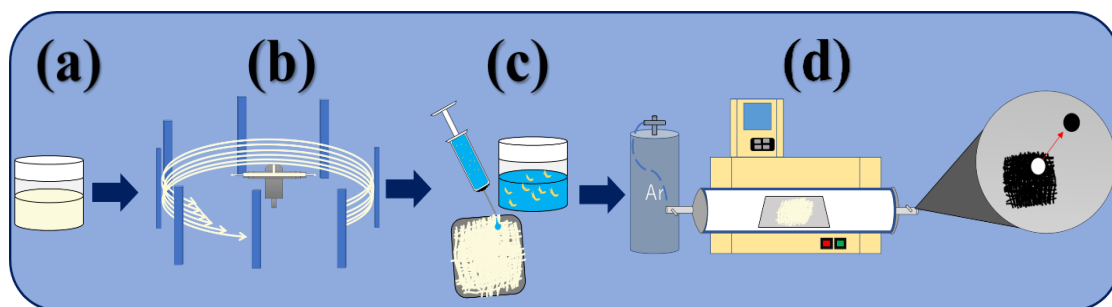


Figure 15. Schematic representation of ceramic/fiber composite anodes fabrication (a) polymer blend solution, centrifugal spinning process (b), coating technique (c), and subsequent heat treatment (d)

3.3 Electrochemical Evaluation

3.3.1 Cell preparation and electrochemical testing

The as-prepared 0.5'' SnO₂ and SnO₂/TiO₂ ceramic/carbon fiber-e anodes were placed in an argon filled glove box (O₂, H₂O concentrations < 0.5 ppm MBRAUN, (USA). Li-ion half cells (CR 2032 (PHD Energy Inc.)), with Li-metal as the counter electrode and glass microfibers as the separator, . The electrolyte was prepared from 1M LiPF₆ in ethylene carbonate (EC)/dimethyl carbonate (DMC) (1:1 v/v) and used without any further additives. Cyclic voltammetry experiments were performed at a scan rate of 0.2 mV s⁻¹ over a voltage range between 0.05 and 3.0 V using Biologic Science Instruments (France).. The electrochemical performance of the anodes was evaluated by galvanostatic charge-discharge experiments using a LANHE battery testing system (CT2001A) with an applied current density of 100 mA g⁻¹ over 70 cycles for the ceramic composites and 100 cycles for the carbonized composites in a potential range of 0.05 – 3.0 V. The rate capability of the composite-fiber anodes was studied using ARBIN with a current density 50 mA g⁻¹, 100, 200, 400, 500, and 50 mA g⁻¹ for 10 cycles each.

CHAPTER IV

RESULTS AND DISCUSSION

4.1 Characterization of ceramic/carbon composites

The precursor fibers were prepared by centrifugal spinning using a FiberLab L1000 (FibeRio) operated at different spinneret rotational speeds. The morphology and elemental composition of the fibers were studied using scanning electron microscope (SEM) using a Sigma VP Carl Zeiss instrument, equipped with an energy dispersive x-ray spectrometer (EDS) from EDAX (Mahwah, NJ, USA)). The thermal behavior of the precursor fibers was investigated by thermogravimetric analysis (TGA) in air environment with temperatures from 50 to 700 °C with a heating rate of 5 °C /min. X-ray diffraction (XRD) and x ray photoelectron spectroscopy (XPS) analyses were performed to determine crystal structure/crystallization phase of the oxidized fibers and the surface chemistry of the fibers. The XRD patterns were studied using a Rigaku Miniflex II X-ray Diffractometer equipped with a copper source (K_{α} λ = 1.54Å). The XPS spectrum were collected using Thermoscientific K- α instrument equipped with monochromatized Al K_{α} radiation (1486.7 eV). Transmission electron microscopy (TEM) images and selected area electron diffraction (SAED) images were captured using a FEI G2 F30 microscope with a working voltage of 300 kV. The High-angle annular dark field (HAADF) scanning TEM (STEM) and EDS maps were acquired with a FEI G2 Titan 60-300 probe corrected microscope equipped with a Super-X EDS system. The Titan was used at 200 kV with a convergence and a HAADF inner collection semi angles of 24mrad and 58.6 mrad, respectively.

4.1.1 Ceramic composite fibers

Figure 16 shows the SEM images of the TiO_2 (a-c), SnO_2 (d-f), $\text{SnO}_2/\text{TiO}_2$ (1:1) (g-i), $\text{SnO}_2/\text{TiO}_2$ (3:2) (j-l) synthesized nano/micro systems obtained after calcination at 700 °C. As it can be seen in Figure 16, the SEM images show short-microfibers morphology. The TiO_2 sample (Fig. 16 (a)) exhibits short fiber porous structure and rough surface composed of spherical particles. On the other hand, the SEM images of the SnO_2 fibers (Figure 16 (d-f)) depict a short fiber morphology with smoother surface and spherical particles randomly embedded in the surface. The $\text{SnO}_2/\text{TiO}_2$ (1:1) composite fibers, also adhere a short-fiber structure morphology with interconnected particles on their surface as can be seen in Figure 16 (g-i). In comparison, the $\text{SnO}_2/\text{TiO}_2$ (3:2) composite fibers show a new microstructure which can be observed in Figure 16(j-l). The SEM images of the $\text{SiO}_2/\text{TiO}_2$ (3:2) composite reveals a short micro belt-fiber structure with spherical particle randomly distributed on the surface.

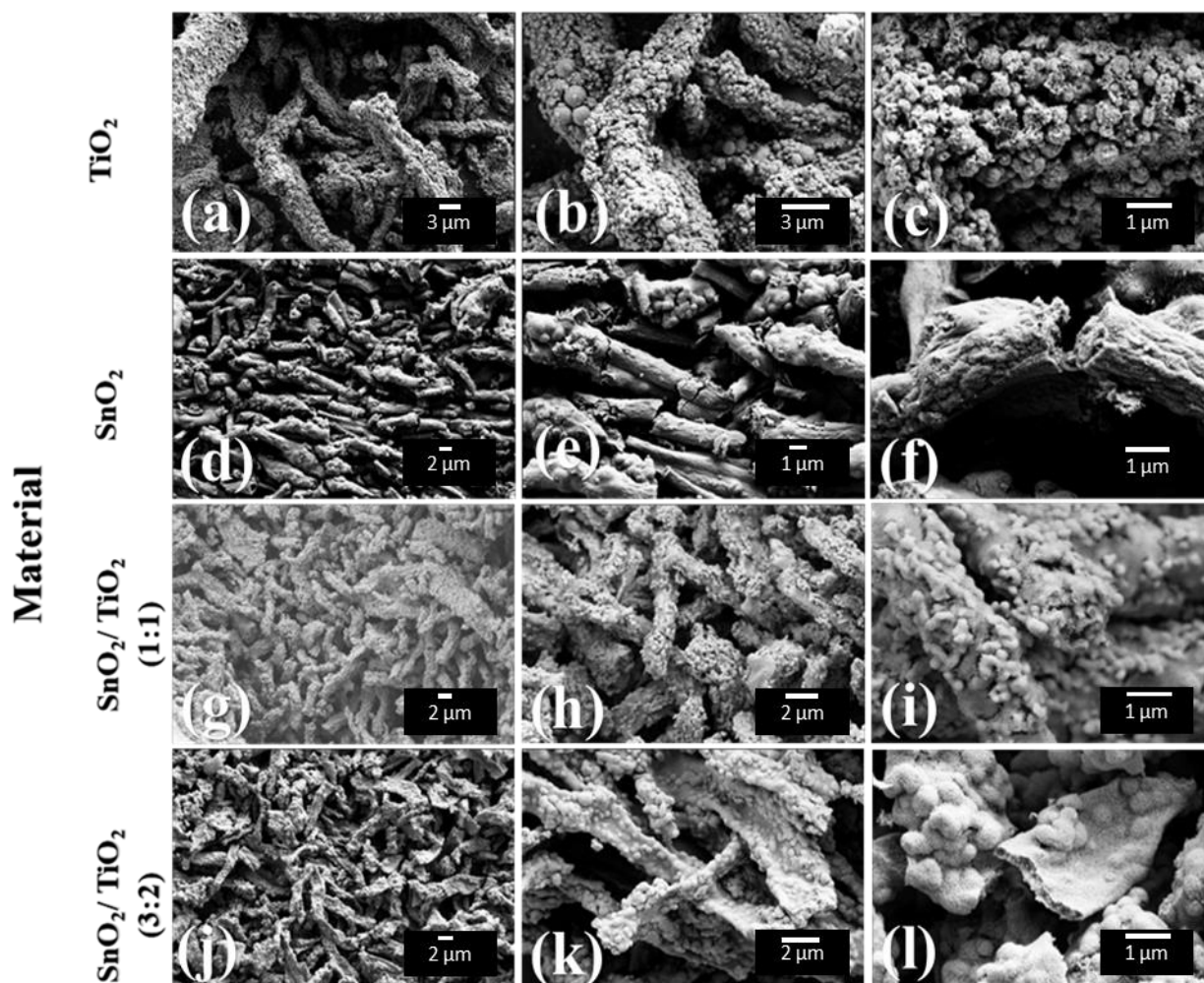


Figure 16. SEM images of TiO_2 (a, b, c), SnO_2 (d, e, f), (1:1) (g, h, i), and $\text{SnO}_2/\text{TiO}_2$ (3:2) (j, k, l), after calcination at 700°C . Magnification: (a, d, g, j) 2000 x, (b, e, h, k) 5,000 x and (c, f, i, l) 10,000 x.

The elemental composition of the composite microfibers was studied by EDS and is shown in Figure 17 (a-d). Sn, Ti, and O can be observed to be highly present within the elemental composition of each corresponding sample. It can be seen in Figure 17 (a) that the TiO_2 sample exhibits a high content of 80 wt. % of Ti while the $\text{SnO}_2/\text{TiO}_2$ composites with 1:1 and 3:2 ($\text{SnO}_2:\text{TiO}_2$) ratios only depict 25 and 18 wt. % of Ti, respectively. Additionally, the pure SnO_2 sample (Figure 17 (b)) shows 90 wt. % of Sn while the $\text{SnO}_2/\text{TiO}_2$ composites with 1:1 and 3:2 ($\text{SnO}_2:\text{TiO}_2$) ratios only demonstrate 52 and 54 wt. % of Sn, respectively. The small

amount of Ti and Sn within the $\text{SnO}_2/\text{TiO}_2$ composite-fiber samples with 1:1 and 3:2 ($\text{SnO}_2:\text{TiO}_2$) ratios are ascribed to the successful mixing of SnO_2 and TiO_2 precursors used to prepare the composite fibers with distinct morphologies. Furthermore, the EDS spectrum of all samples also exhibits signal peaks of oxygen, which confirm the presence of SnO_2 and TiO_2 in the as-synthesized samples. Moreover, carbon and nitrogen signals can also be observed in all samples. However, such insignificant signals found in the elemental composition can be attributed to precursor impurities, carbon residue from the PVP, and the carbon tape used during sample preparation [78].

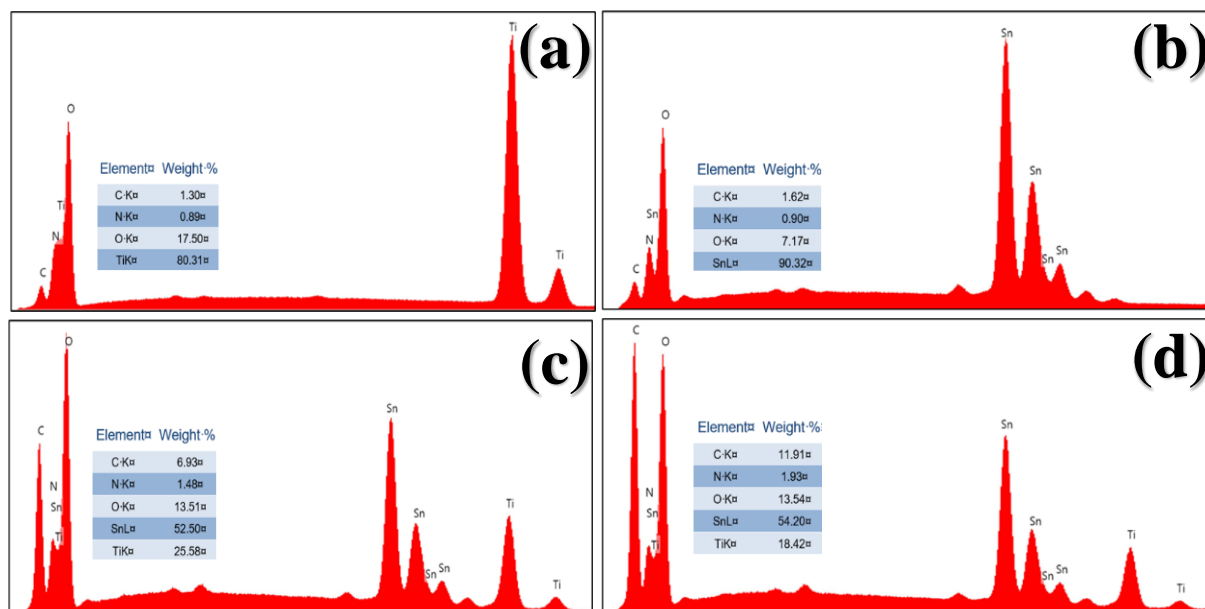


Figure 17. EDS spectrum of TiO_2 (a) SnO_2 (b), $\text{SnO}_2/\text{TiO}_2$ (1:1) (c), and $\text{SnO}_2/\text{TiO}_2$ (3:2) (d) after calcination at 700 °C.

Figure 18 (a) shows the TGA results of the composite precursor fibers as well as the XRD (b) of the fibers. As can be seen in the figure, all composite precursor fibers have two main weight loss -steps observed in two different temperature ranges. The first weight loss was observed in the range of 25 -100 °C which can be attributed to the loss of either remaining solvent or water adsorbed within the fibers. The second observed weight loss between 300 and 550 °C

can be associated with the degradation of the polymer and ceramic precursor-fibers. At the temperature range between 560 and 700 °C, the samples show stable and constant average of residual weight of 10 wt. %, which was attributed to the formation of SnO₂, TiO₂, and SnO₂/TiO₂ composites as well as carbon residue, impurities from the polymer. Figure 4b shows diffraction patterns for the SnO₂ (i), TiO₂ (ii), SnO₂/TiO₂ (1:1) (iii), and SnO₂/TiO₂ (3:2) (iv) short microfibers. The SnO₂ (i) and TiO₂ (ii) samples have similar lattices which was the P42/M space group and each lattice has different lengths to the sides of the unit cell. The results of the Le Bail fitting is shown in Table 1 which indicate that a good fitting was obtained between the known structure of TiO₂ and SnO₂ and the synthesized samples; the GOF is indicated by a χ^2 value of less than 5. The TiO₂ diffraction pattern showed peaks at 2 θ of 32.1, 42.3, 45.8, 48.3, 51.6, 64.3, 67.0, 74.6, and 76.1°. These diffraction peaks correspond to the 110, 101, 200, 111, 210, 211, 220, 002, 310, 221 diffraction planes for the rutile phase of TiO₂. The diffraction pattern for the SnO₂ (Figure 18b (i)) showed diffraction peaks at 31.0, 39.7, 44.6, 45.6, 61.00, 64.8, 68.9, 73.6, 74.3, 77.1 and 78.8°, which correspond to the 110, 101, 200, 111, 210, 211, 220, 002, 310, 221, 112, 301 diffraction planes. The XRD patterns of the SnO₂/TiO₂ short fibers showed diffraction peaks at 31.2, 40.3, 44.5, 61.7, 65.0, 74.00 and 78.5° which correspond to a combination of the diffraction planes observed for the SnO₂ and TiO₂ materials. The fitting results confirmed both rutile (TiO₂) and SnO₂ [79-81] [82, 83]. In addition, the observed diffraction peaks in the composite-fiber samples were broad and relatively weak, indicating a smaller particle size for both TiO₂ and SnO₂ when compared to the individual particles of TiO₂ and SnO₂.

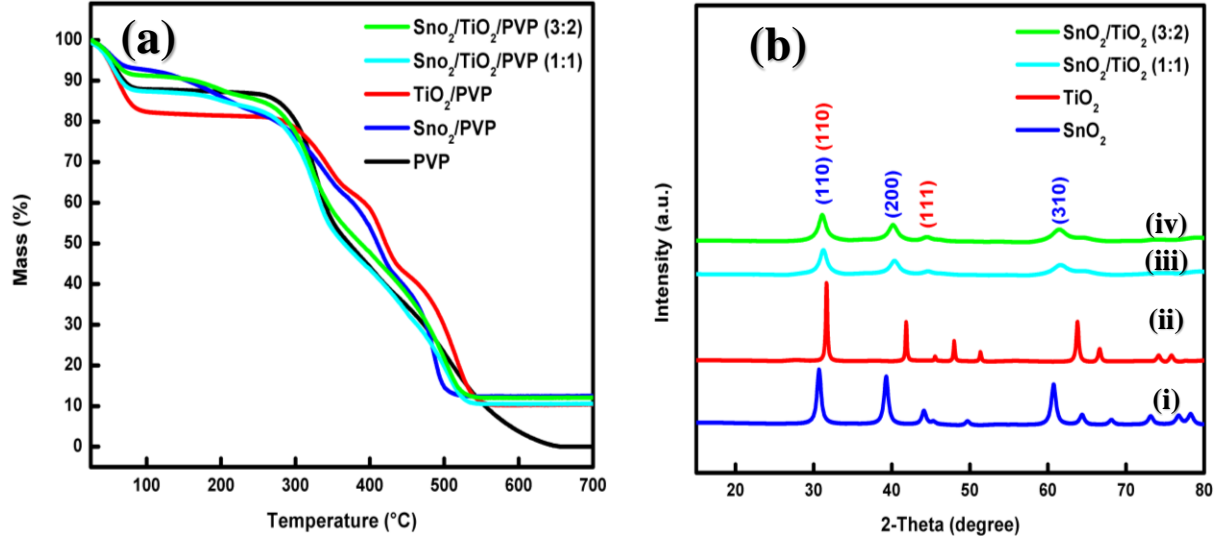


Figure 18. TGA (a) of PVP and pristine fibers before calcination, XRD (b), of TiO_2 (i), SnO_2 (ii), $\text{SnO}_2/\text{TiO}_2$ (1:1) (iii), and $\text{SnO}_2/\text{TiO}_2$ (3:2) (iv) after calcination at 700 °C.

Table 1: Le Bail fitting SnO_2 , TiO_2 and $\text{SnO}_2/\text{TiO}_2$ samples

Sample	Phase	Space Group	a(Å)	b(Å)	c(Å)	$\alpha(^{\circ})$	$\beta(^{\circ})$	$\gamma(^{\circ})$	χ^2
SnO_2 700°C	SnO_2	P 42/m n m	4.732(7)	4.732(7)	3.132(9)	90.00	90.00	90.00	2.44
TiO_2 700°C	TiO_2	P 42/m n m	4.589(9)	4.589(9)	2.957(2)	90.00	90.00	90.00	3.04
	TiO_2	P 42/m n m	4.600(2)	4.600(2)	2.98(2)	90.00	90.00	90.00	
$\text{SnO}_2/\text{TiO}_2$ 700°C 1:1	TiO_2	P 42/m n m	4.518(1)	4.518(1)	2.959(2)	90.00	90.00	90.00	2.08
	SnO_2	P 42/m n m	4.7454(4)	4.745(4)	3.130(9)	90.00	90.00	90.00	
$\text{SnO}_2/\text{TiO}_2$ 700°C 3:2	TiO_2	P 42/m n m	4.544(2)	4.544(2)	2.950(0)	90.00	90.00	90.00	1.82
	SnO_2	P 42/m n m	4.741(6)	4.741(6)	3.133(9)	90.00	90.00	90.00	

X-ray photoelectron (XPS) characterization was performed to determine the compositions and chemical states of the elemental components in the as synthesized samples. The XPS survey spectrum for each sample is shown in Figure 19 (a-d), which shows the presence of Sn and O as the major components in the SnO_2 sample and some residual C from the sample preparation. The XPS spectrum of the TiO_2 fibers shows the presence of Ti and oxygen as the main portions of the sample with some residual carbon left from the synthesis. The $\text{TiO}_2/\text{SnO}_2$ composite-fiber samples consisted of Ti, Sn and O as well as a small amount of C residue from the sample preparation.

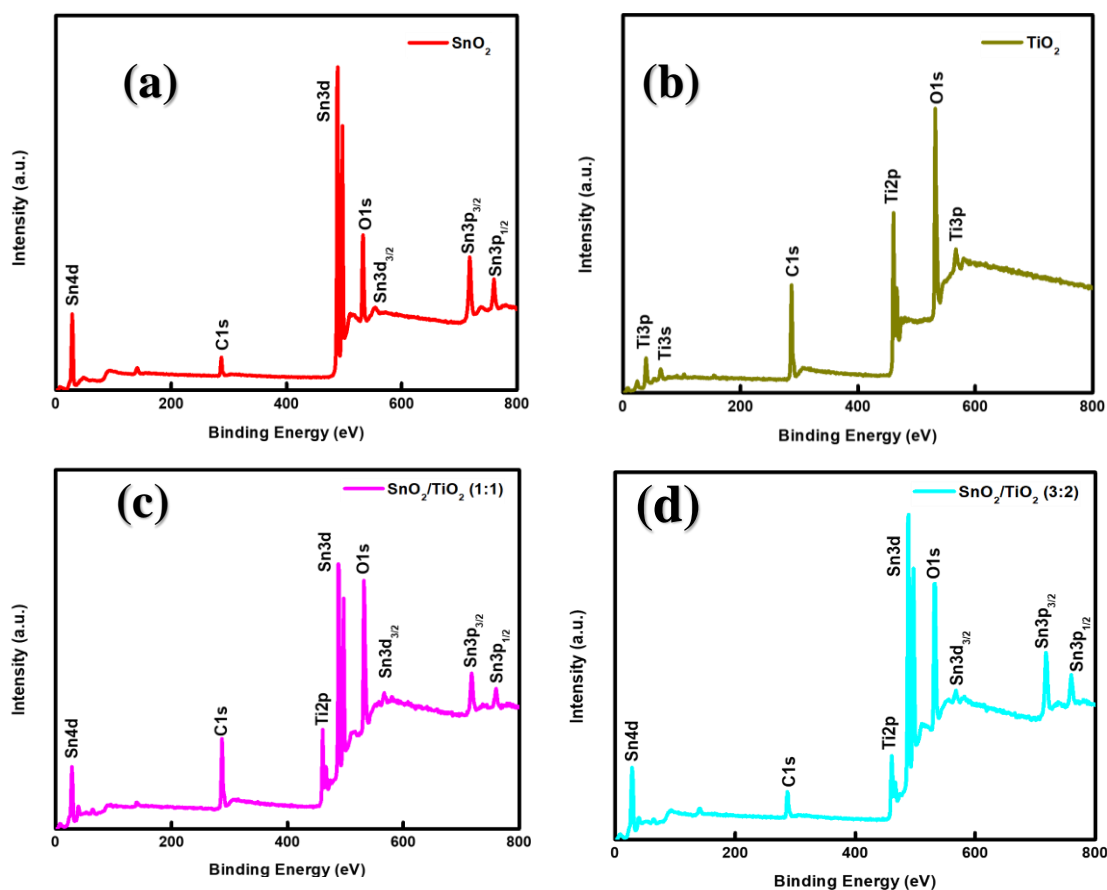


Figure 19. XPS surveys for the SnO_2 oxidized short fibers at 700°C (a), $\text{SnO}_2:\text{TiO}_2$ with a ratio of 1:1 (b), and $\text{SnO}_2:\text{TiO}_2$ at a ratio of 3:2 (c).

Figure 20 shows the Sn 3d_{5/2} and 3d_{3/2} peaks, which are located around 487 eV and 496 eV, respectively. Figure 20 (a) shows the spectrum for the SnO₂ oxidized at 700°C the spectrum can be deconvoluted into 2 peaks. In the Sn 3d_{5/2}, a small peak is observed at 487 eV indicating the presence of Sn (IV) [84-86]. The second peak observed in the spectrum is the Sn3d_{3/2} fitting which was located at 495.2 eV again indicating the presence of Sn (IV) in the sample. Figure 20 (b) and (c) show the XPS spectrum of the oxidized SnO₂/TiO₂ composite fibers with a ratio of 1:1 and 3:2, respectively. The XPS results in Figure 6 b and c showed the presence of Sn 3d_{5/2}.

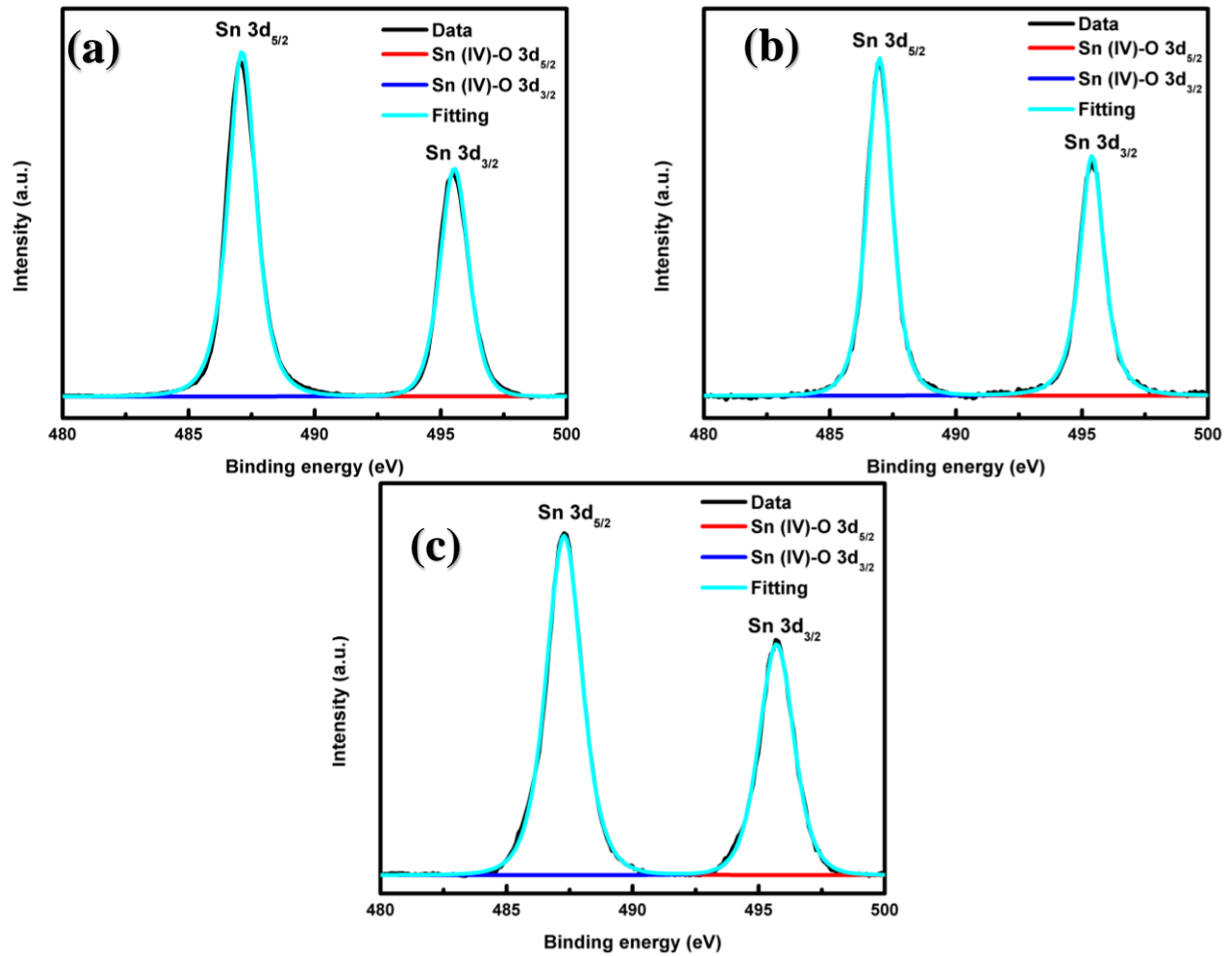


Figure 20. Sn 3d XPS for the SnO₂ oxidized short fibers at 700°C (a), SnO₂:TiO₂ with a ratio of 1:1 (b), and SnO₂:TiO₂ at a ratio of 3:2(c).

Figure 21 (a) shows the Ti 2P_{5/2} and Ti2P_{3/2} XPs regions for the TiO₂ and SnO₂/TiO₂ composite-fiber samples after heat treatment at 700°C. Figure 21 (a) shows the Ti₂P XPS spectrum for the pristine TiO₂ fibers oxidized at 700 °C which was deconvoluted into three peaks located at 459.2, 464.9 eV and 472.6 eV. The peaks located at 459.2 and 464.9 eV are the Ti 2P_{5/2} and Ti2P_{3/2} and confirm the presence of Ti as Ti(IV) in the TiO₂ fibers [86-88]. The third peak located around 472.6 eV was determined to be the Ti 2P satellite feature [86, 88]. In addition, the SnO₂/TiO₂ (1:1) and (3:2) show the same peaks with the same energies indicating the presence of Ti in all the fibers contained Ti(IV) as TiO₂. Figure 21 (b) and (c) show the Ti 2P spectrum for the SnO₂/TiO₂ composite fibers with SnO₂ toTiO₂ ratios of 1:1 and 3:2, respectively. The Ti 2P spectra in Figure 21 (a) and (b) again show three peaks, which are located at 459.2 and 464.9, and 472.6 eV and represent the Ti 2P_{5/2}, Ti2P_{3/2}, and Ti 2P satellite, respectively. The XPS spectra in Figure 21 (b and c) show the presence of Ti in the TiO₂/SnO₂ composite fibers, which was present as Ti(VI).

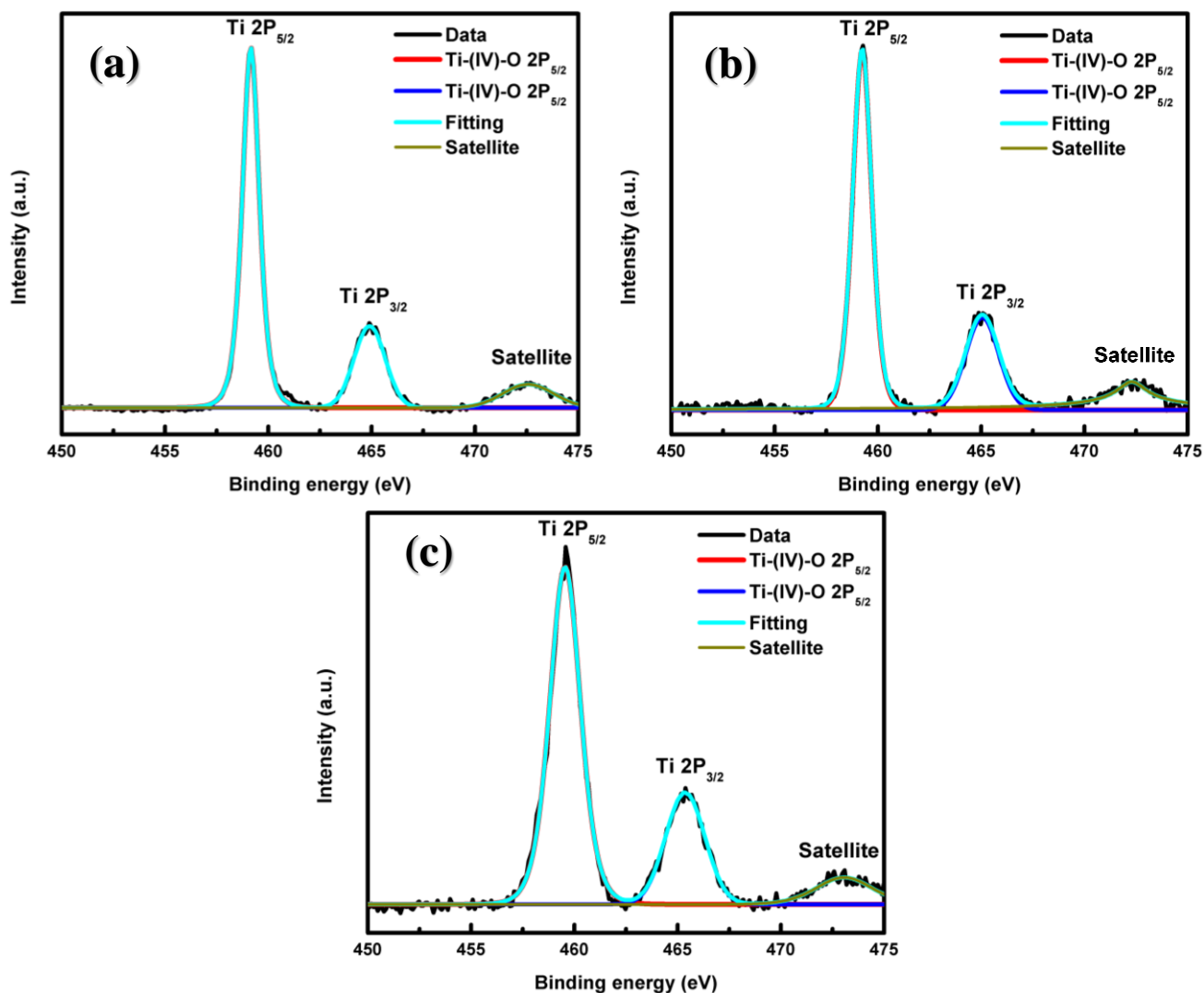


Figure 21. Ti 2P XPS spectrum of TiO_2 oxidized at 700°C (a), $\text{SnO}_2\text{:TiO}_2$ at a ratio of 1:1 (b), and $\text{SnO}_2\text{:TiO}_2$ at a ratio of 3:2 (c).

Figure 22 (a-d) shows the O 1S XPS spectrum for the as synthesized SnO_2 , TiO_2 and $\text{SnO}_2/\text{TiO}_2$ fibers. Figure 22 (a) shows the spectrum for SnO_2 fibers oxidized at 700°C which was deconvoluted into two peaks, which were located at 531 and 532 eV. The two peaks located at 531 and 532 eV are indicative of oxygen bound to a high oxidation state metal such as Sn(IV) and the presence of hydroxide in the sample [88-90]. Figure 22 (b) shows the O1S spectrum for the TiO_2 fibers, which was similarly deconvoluted into two peaks located at 530 and 532 eV indicating the presence of a high oxidation state metal and the presence of hydroxide. The O1S

spectrum of the $\text{SnO}_2/\text{TiO}_2$ composite fibers with SnO_2 to TiO_2 ratios of 1:1 and 3:2 is shown in Figures 22 (c) and 22 (d), respectively. The XPS results for the $\text{SnO}_2/\text{TiO}_2$ composite fibers showed the presence of two peaks in the O1s spectrum indicating metal-oxygen and the metal-hydroxide bonds, which are located 531 and 532 eV, respectively, as was shown in the in the TiO_2 and SnO_2 individual samples.

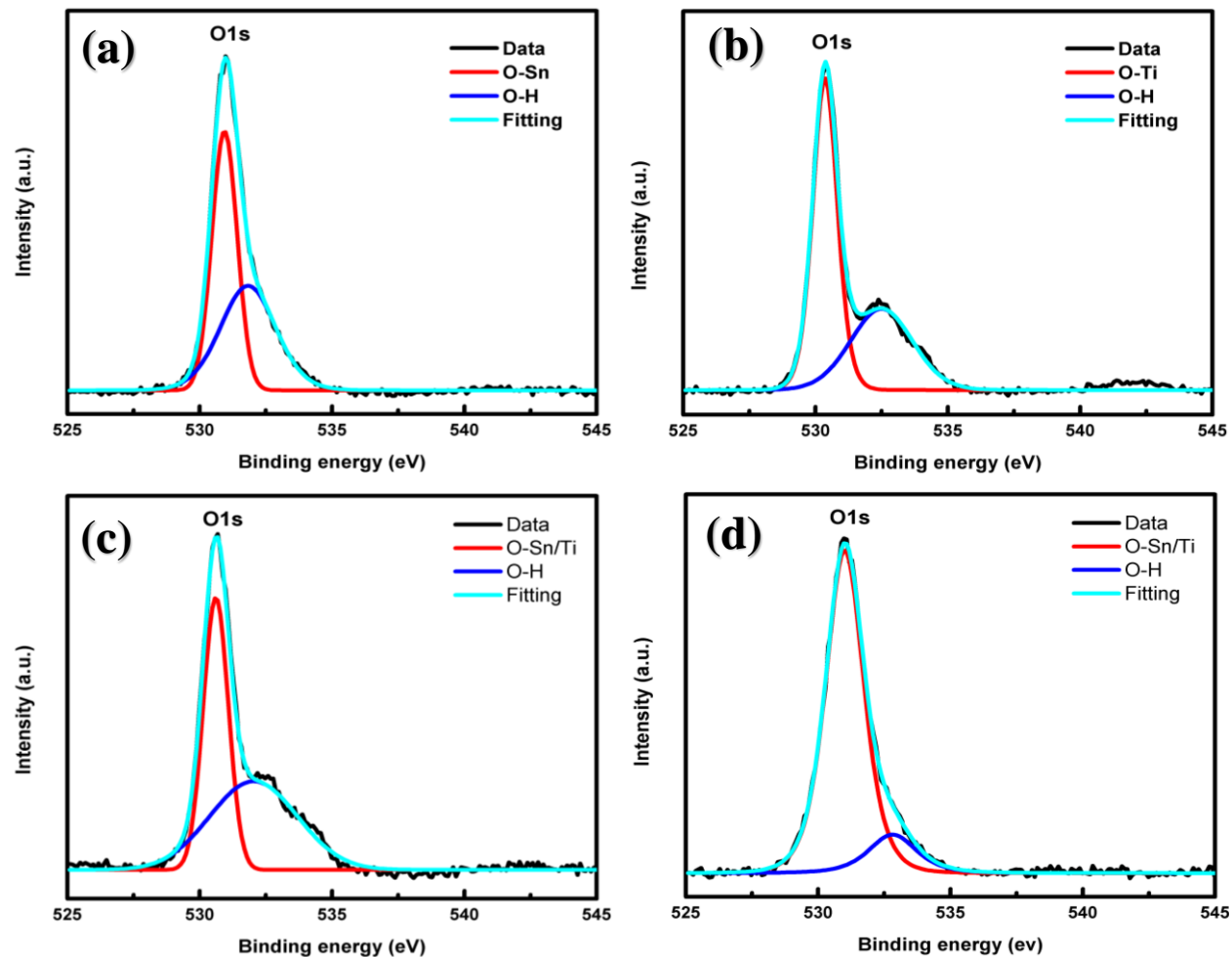


Figure 22. O1s XPS spectrum of TiO_2 oxidized at 700°C (a), $\text{SnO}_2:\text{TiO}_2$ at a ratio of 1:1 (b), and $\text{SnO}_2:\text{TiO}_2$ at a ratio of 3:2 (c).

4.1.2 Ceramic/carbon fiber composites

To study the surface morphology and structure of the carbonized ceramic/carbon composite fibers, SEM images were taken at 5,000 and 15,000 magnification (Figure 23). It can be seen in Figure 23 (a-f) show the SEM images for the ceramic/carbon composite fibers. It can be observed in Figure 23 (a, b) that when the coating with pure SnO_2 ceramic fibers, the short-fiber morphology disappeared and instead, spherical particles were embedded on the surface of the FPCFs. In comparison, when using the ceramic composite fibers with 1:1 (SnO_2 : TiO_2) ratio to coat the FPCFs, spherical particles embedded on the surface as well as small nanoflakes on the surrounding can be observed. Similarly, when coating FPCFs with the composite with (3:2) (SnO_2 : TiO_2) ratio, the spherical particles were no longer visible and instead nanoflakes were formed on spherical particles and are deposited on the surface of the FPCFs (Figure 23 (e,f)). Although the short fiber structure was lost, the presence of Sn, Ti, and O is still present within the composite fibers as shown by the EDS spectra of each corresponding sample in figure 24(a-c). Moreover high concentrations of C and N are also observed and can be attributed to the carbonized fibers that were incorporated.

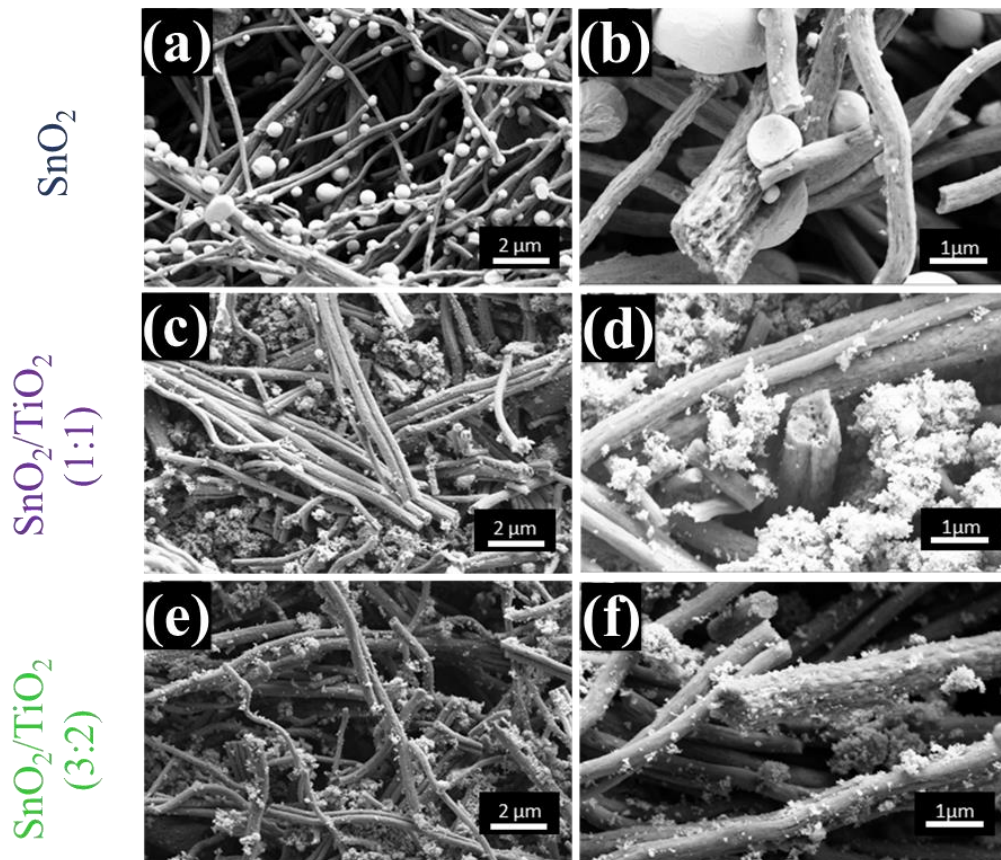


Figure 23. SEM images of SnO_2 /FPCFs (a, b), $(1:1) \text{SnO}_2:\text{TiO}_2$ /FPCFs (c, d), $(3:2) \text{SnO}_2:\text{TiO}_2$ /FPCFs (e, f) ceramic/carbon composite fibers at a 5,000 x, 15,000 x magnification.

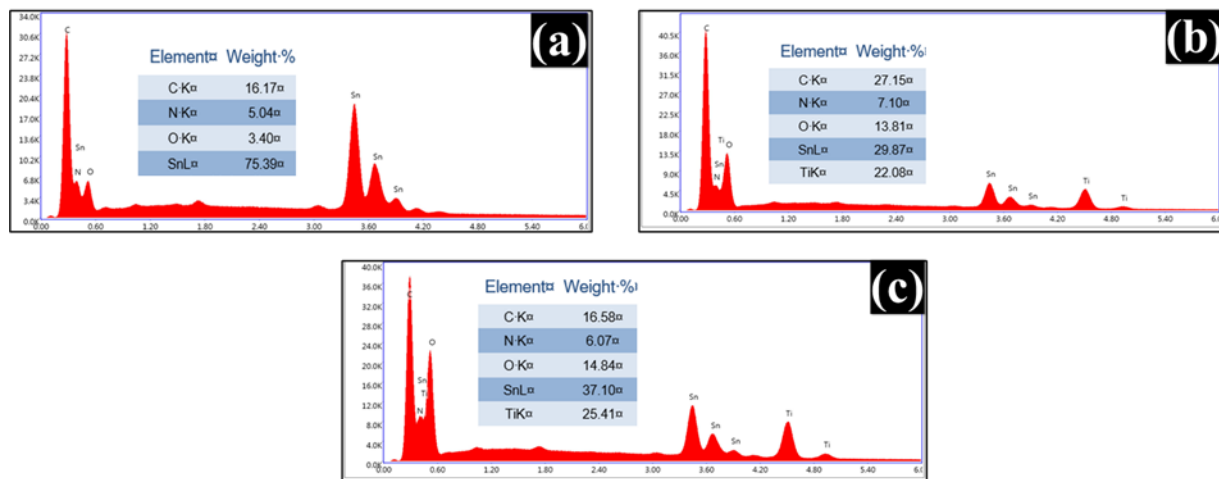


Figure 24. EDS spectra of SnO_2 /FPCFs (a), $(1:1) \text{SnO}_2:\text{TiO}_2$ /FPCFs (b), $(3:2) \text{SnO}_2:\text{TiO}_2$ /FPCFs (c) ceramic/carbon composite fibers

The crystal structure and thermal decomposition of the coated fibers were studied by XRD and TGA, respectively. The diffraction peaks at 35, 38, 50, 53, 65, 74, 75, 77° in 2 θ are observed in all the ceramic/carbon samples and are attributed to the presence of metallic Sn, indicating the reduction of SnO₂ to Sn after the subsequent heat treatment [27, 31, 91, 92]. Furthermore, the peak at 33° is only present in the SnO₂:TiO₂ samples and can be assigned to presence of rutile TiO₂ within the composites[82, 83, 93]. To investigate the amount of active material retained within the fibers after the carbonization process, TGA experiments (Figure 25b) were performed from 25 to 700 °C at 5 °C/min in air. It is obvious that both, the uncoated and coated FPCFs, exhibit two major-steps losses. The first step loss occurs at 25-250 °C for the FPCFs, at 25-180 °C for the coated FPCFs, and can be attributed to the evaporation of any remaining solvent in the sample. The next step loss can be identified at a temperature range of 440-600 °C for the FPCFs and at 380-500 °C for the coated FPCFs. The residual mass of ~3% for the FPCFs can be attributed to the graphitized residual carbon from the PAN as well as polymer impurities. On the other hand, the residual masses of 52, 53, and 48 % observed for the coated FPCFs represented the amount of SnO₂ and SnO₂/TiO₂ remained in the samples after carbonization.

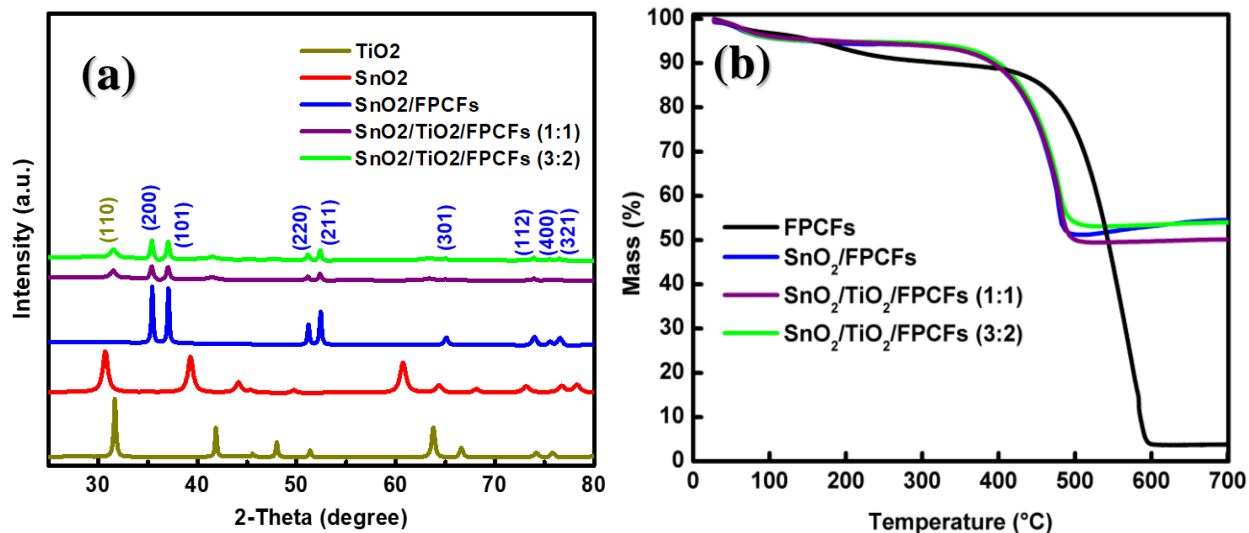


Figure 25. TGA (a) and XRD (b) of TiO₂ (i), SnO₂ (ii), ceramic fibers and SnO₂/FPCFs (iii), SnO₂/TiO₂ (1:1)/FPCFs (iv), SnO₂/TiO₂ (3:2)/FPCFs (v) ceramic/carbon composite fibers.

X-ray photoelectron (XPS) characterization was conducted to study the composition and chemical states of the synthesized ceramic/carbon composites. The XPS survey spectrum for each sample is shown in Figure 26 (a-c), which shows the presence of Sn and O as the major components in the SnO₂/FPCFs sample, as well as some carbon and nitrogen attributed to the presence of the carbon fiber matrix. The SnO₂/TiO₂ composite-fiber samples consisted of Ti, Sn and O as well as carbon and nitrogen. Such results confirm the successful coating of the pure ceramic fibers onto the flexible and porous carbon fibers.

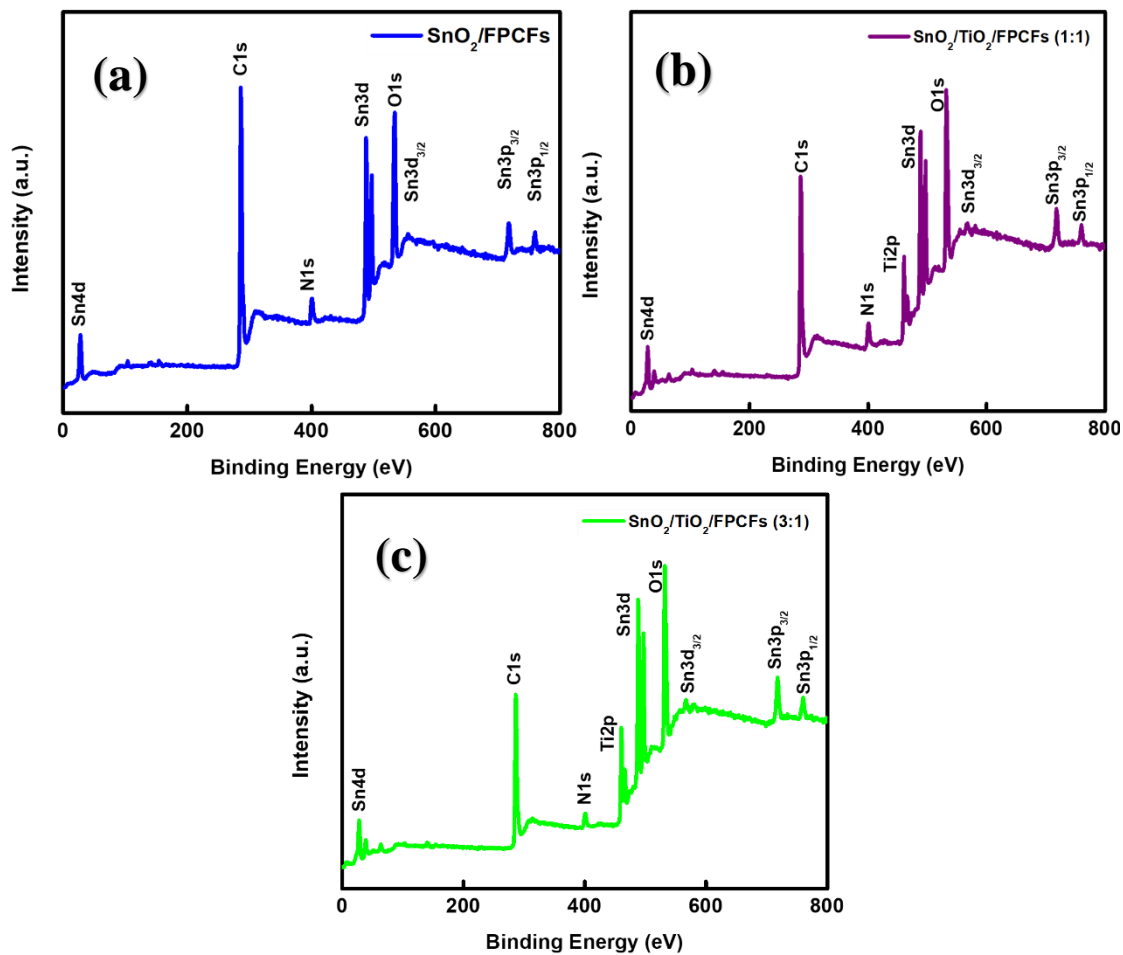


Figure 26. XPS surveys of $\text{SnO}_2/\text{FPCFs}$ (a), (1:1) $\text{SnO}_2:\text{TiO}_2/\text{FPCFs}$ (b), (3:2) $\text{SnO}_2:\text{TiO}_2/\text{FPCFs}$ (c) ceramic/carbon composite fibers

4.2 Electrochemical Performance

To study the electrochemical performance of the ceramic/carbon composite fibers various electrochemical analyses were conducted. The cycling capability was studied by galvanostatic charge-discharge testing at a current density of 100 mA g^{-1} over a voltage potential range of 0.05-3.0 V. In addition, the rate performance of the composites was also investigated at different current densities to study the rate capability of the short fibers. Furthermore, cycling voltammetry (CV) experiments were conducted at room temperature to study the redox reactions within the composites and they were performed at a voltage range of 0.01-3 V with a scan rate of 0.02 mVs^{-1} over 4 cycles. The resistance across the cell was also measured conducting electrochemical impedance spectroscopy (EIS).

4.2.1 $\text{SnO}_2/\text{TiO}_2$ ceramic composite fibers

To determine the reduction/oxidation reactions of the anode electrode, CV experiments were performed over a voltage range of 0.05 -3.0 V and at a scan rate of 0.2 mVs^{-1} over four cycles. Figure 27 shows the cyclic voltammetry curves of the $\text{SnO}_2/\text{TiO}_2$ ceramic composites.

During the first cycle, the peaks at 0.95, 0.11, and the peak between 0.5-1 V can be attributed to the formation of the solid electrolyte interface (SEI), electrolyte decomposition, and the dealloying process generating Li_xSn , respectively [33, 94, 95]. Furthermore, the redox peak at 1.3 V is ascribed to the reversible conversion reaction of Sn and LiO_2 to form SnO_2 while the peak at 1.89 V is attributed to the insertion/ extraction of lithium from TiO_2 . From the second cycle and beyond, the CV curves coincide with each other, indicating high reversibility and good cycling performance of the anode electrode. The process illustrated by the CV curves can be chemically represented by the following equations [33, 94, 95]:

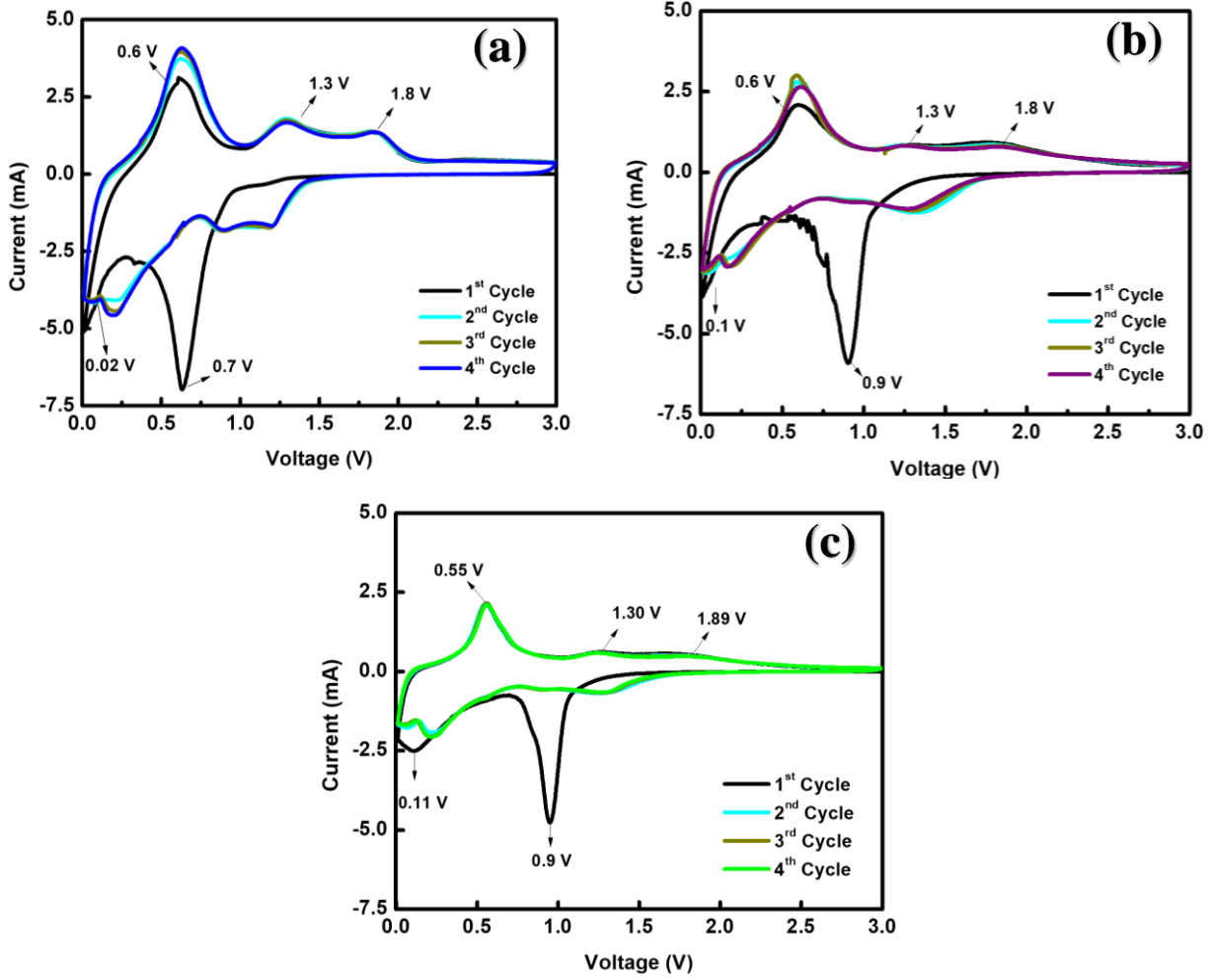
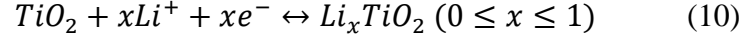
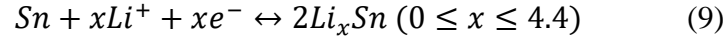
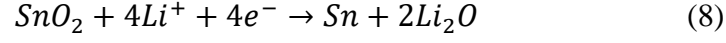


Figure 27. Cyclic voltammetry of ceramic fibers from SnO₂(b), SnO₂:TiO₂ at a ratio of (1:1) (c) and at a ratio of SnO₂:TiO₂ at a ratio of (3:2) (d).

The cycle performance of the SnO₂/TiO₂ ceramic fibers was evaluated using galvanostatic experiments at a current density of 100 mA g⁻¹ for 70 cycles over a voltage range of 0.05-3.0 V (Figure 28 (a, b) and (c, d), respectively). Initially, the SnO₂ ceramic fibers demonstrated irreversible discharge capacity of 1123 mAh g⁻¹ and charge capacity of 741 mAh g⁻¹; however, the reversible capacity after 70 cycles dropped to 179 mAh g⁻¹. Such a capacity reduction has been attributed to the pulverization and instability of SnO₂ upon cycling caused by the high-volume change developed during lithium insertion/extraction. In comparison, the SnO₂/TiO₂ at a (1:1) ratio demonstrated the lowest capacity after 70 cycles. Due to its excessive amount of TiO₂ the final capacity resulted in 244 mAh g⁻¹. On the other hand, the SnO₂/TiO₂ micro-belt fibers (3:2 ratio) demonstrated high but irreversible discharge capacity of 1200 mAh g⁻¹ and charge capacity of 820 mAh g⁻¹ during the first cycle, resulting in a coulombic efficiency of 65 %. Such irreversible capacity can be attributed to the formation of the SEI at the anode/electrode interface. At the second cycle, the reversible capacity decreased to 700 mAh g⁻¹ which was twice than that of graphite; however, after 70 cycles the capacity decreased to 279 mAh g⁻¹. Such a drastic drop in capacity can be attributed to inevitable pulverization of the anode upon cycling caused by internal stresses (volume change) during lithiation/de-lithiation. Despite this performance, the electrode retained a high coulombic efficiency of 99% indicating good reversibility. When comparing the pure SnO₂ ceramic fibers to the SnO₂/TiO₂ composite fibers with a ratio of 1:1 and 3:2 (Fig.28 (a, b)), it was obvious that the SnO₂/TiO₂ short fibers demonstrated less volume expansion due to the addition of TiO₂ and also to its unique micro-belt structure. Such attributes mitigated the internal stresses experienced upon cycling which resulted in better capacity retention and higher reversible capacity after 70 cycles. More work is needed to improve the electrochemical performance of the SnO₂/TiO₂ short-fiber anode.

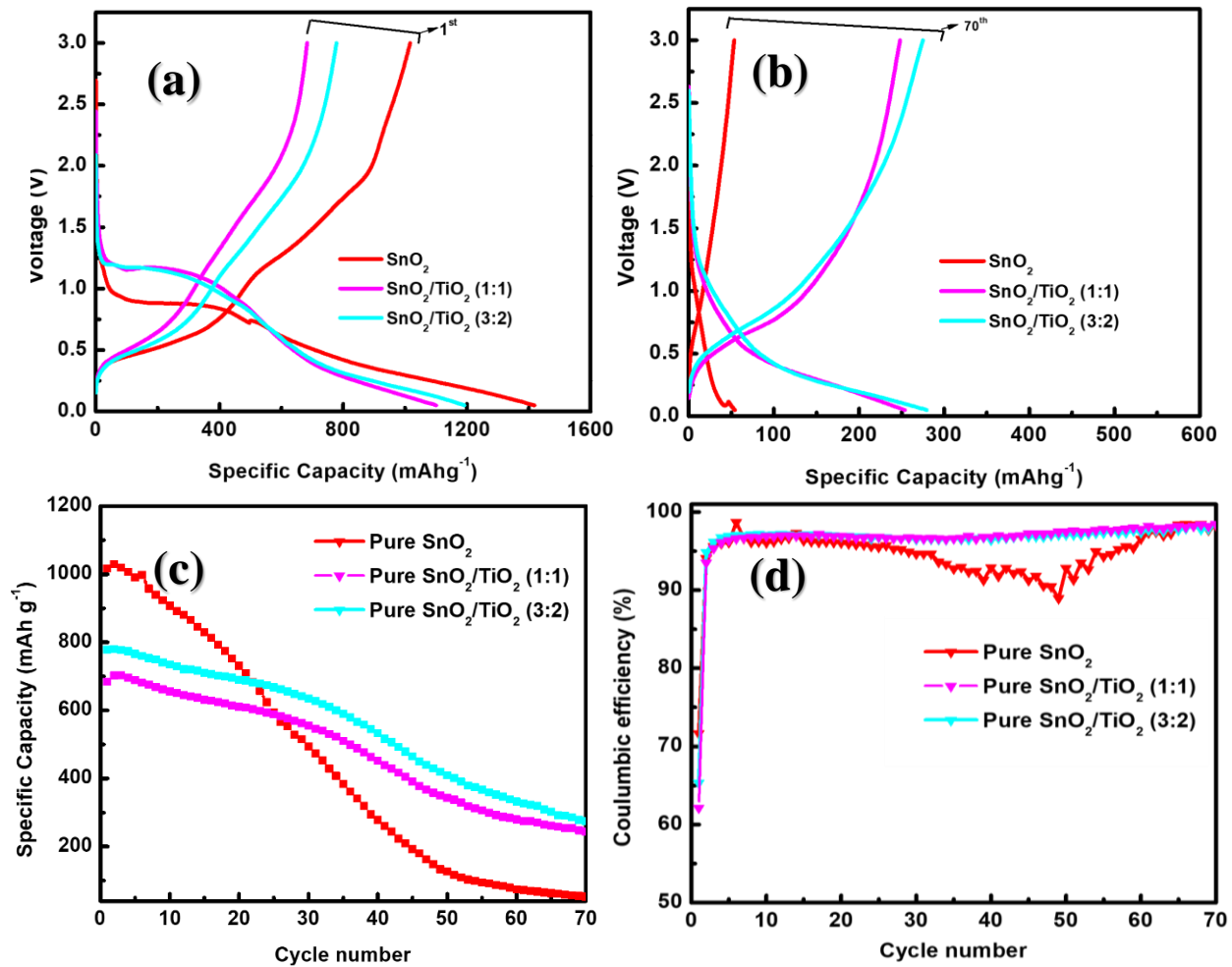


Figure 28. Charge/discharge curves of the SnO_2 , (1:1) $\text{SnO}_2/\text{TiO}_2$, (3:2), $\text{SnO}_2/\text{TiO}_2/\text{FPCFs}$ at the 1st (a) and 100th (b) as well as the charge capacity (c) and coulombic efficiency (d) after 100 cycles at a current density of 100 mA g^{-1} .

To further investigate the electrochemical performance and reversibility of the composites, the $\text{SnO}_2/\text{TiO}_2$ micro-belt fibers anodes with a ratio of 3:2 were tested at different current rates (the rate performance results are shown in figure 29). It can be observed that the $\text{SnO}_2/\text{TiO}_2$ micro-belt fibers delivered a high initial capacity of 723 mAh g^{-1} attributed to its high content of SnO_2 which yields high capacities. Moreover when the current density reached 500 mA g^{-1} , the micro-belt fibers retained a capacity of 250 mAh g^{-1} accredited to the addition of TiO_2 that serves a buffer for volume expansion. However, when the current rate is brought back to 50 mA g^{-1} the composite returns a capacity of only 470 mAhg^{-1} , indicating a

poor reversibility. Such results can be attributed to its brittle properties that cause the material to pulverize over prolonged cycling.

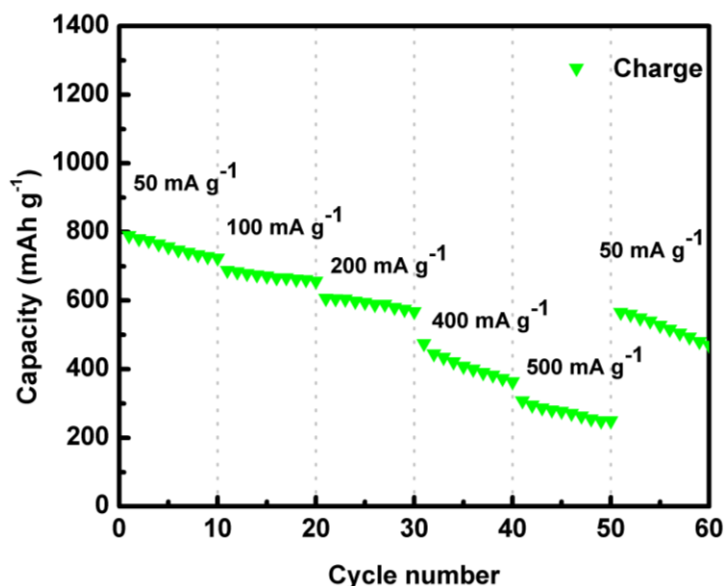
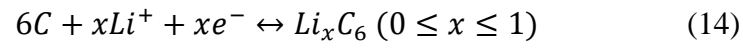
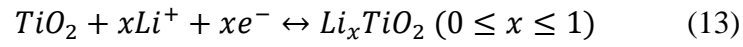
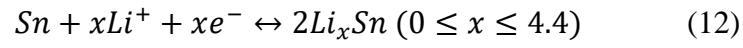
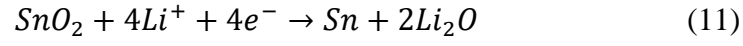


Figure 29. Rate performance of SnO₂/TiO₂ short-fiber (3:2 ratio) anode.

4.2.2 Ceramic/carbon fiber composites

To study the lithiation/delithiation reactions of the anodes, CV tests were performed for 4 cycles over a voltage potential window of 0.05- 3 V and a scan rate of 0.2 mVs⁻¹. Figure 30 shows the CV curves for the SnO₂:TiO₂/FPCFs composites. During the first cycle, three main reduction peaks are visible at 1, 0.7, and 0.3 V. These peaks represent the breakdown of electrolyte, the SEI layer formation, and the alloying reaction between Li and Sn, respectively. Additionally, the oxidation peaks at 0.65, 0.75, 0.8 V are ascribed to the dealloying of Li_xSn, while the broad peak at 1.2 V represents the extraction of lithium from the carbon and overlaps with the peak at 1.3 V that corresponds to the insertion/extraction of lithium from titanium. [25, 26, 28, 92, 96, 97]. Moreover, Equation 11 represents the irreversible reaction of SnO₂ with LiO₂ to form Li_xSn, which contributes to the first irreversible capacity. Equation 12 is ascribed to the reversible capacity that results from the alloying/dealloying of Sn and Li. Equation 13 illustrates

the insertion/extraction reaction which is attributed to the interaction between lithium and TiO_2 while Equation 14 represents the interaction between Li and the carbon fibers. After the first cycle, the CV curves overlap each other, indicating good capacity reversibility of the $\text{SnO}_2\text{:TiO}_2\text{/FPCFs}$ composite anode.



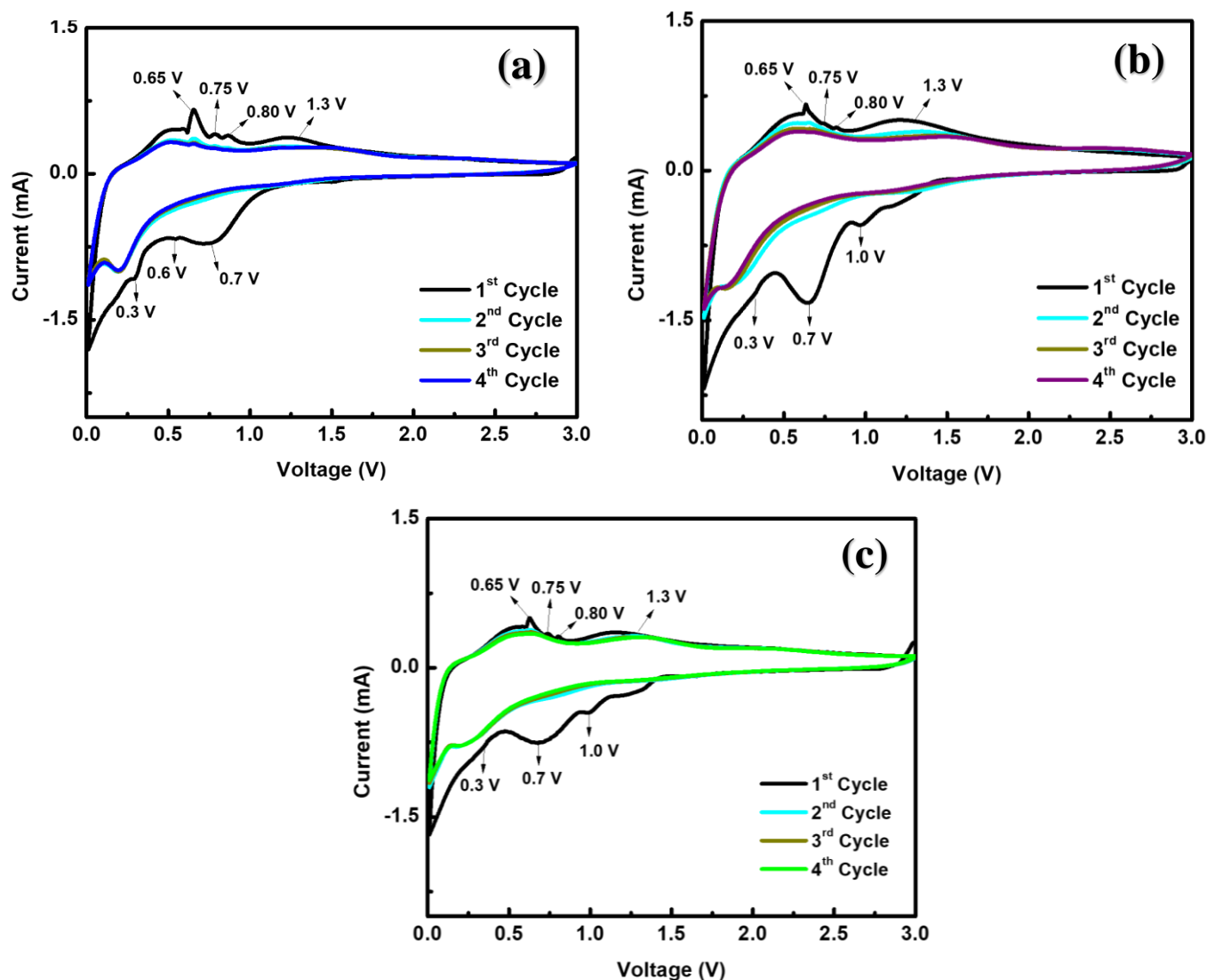


Figure 30. CV curves of $\text{SnO}_2/\text{FPCFs}$ (a, b), $(1:1) \text{SnO}_2:\text{TiO}_2/\text{FPCFs}$ (c, d), $(3:2) \text{SnO}_2:\text{TiO}_2/\text{FPCFs}$ (e, f) ceramic/carbon composite fibers

To investigate the electrochemical performance of the $\text{SnO}_2/\text{FPCFs}$, $(1:1) \text{SnO}_2:\text{TiO}_2/\text{FPCFs}$, and $(3:2) \text{SnO}_2:\text{TiO}_2/\text{FPCFs}$, galvanostatic charge/discharge experiments were performed at a current density of 100 mA g^{-1} from 0.05-3.0V for 100 cycles. Figures 31 (a, b) show the cycling performance of the ceramic/carbon composite fibers after the 1st and 100th cycle. At the 1st cycle, the $\text{SnO}_2/\text{FPCFs}$, $(1:1) \text{SnO}_2:\text{TiO}_2/\text{FPCFs}$, and $(3:2) \text{SnO}_2:\text{TiO}_2/\text{FPCFs}$ delivered a discharge capacity of 1903, 1920, and 1839 mAh g^{-1} , respectively. Such large

capacities can be accredited to the high theoretical capacity of Sn/SnO₂ as well as the large number of Li-ions intercalated with carbon in the porous carbon-fiber matrix during the first cycle. However, such high capacities are also irreversible due to the formation of the SEI layer that takes a substantial amount of Li-ions as it forms on the anode surface. For this reason, the charge capacity of ceramic/carbon composite fibers decreased to 1290, 1240, and 1197 mAh g⁻¹, resulting in a low coulombic efficiency of 67, 64, and 65 %, for the SnO₂ /FPCFs, (1:1) SnO₂:TiO₂/FPCFs, and the (3:2) SnO₂:TiO₂/FPCFs, respectively (Figure 31 d). However, after the second cycle, the coulombic efficiency increases to 98 % for all ceramic/carbon composites and remains stable, indicating good reversibility of the porous carbon fibers. After 100 cycles, the (3:2) SnO₂:TiO₂/FPCFs delivered a reversible capacity of 890 mAh g⁻¹ while the SnO₂ and (1:1) SnO₂:TiO₂/FPCFs anodes exhibited a capacity of 877, and 840 mAh g⁻¹, respectively. As shown in Figure 31 (c), though the capacity of the (3:2) SnO₂:TiO₂/FPCFs composite was slightly higher, the overall cycling stability demonstrated by this composite was better than that of the SnO₂/FPCFs and the (1:1) SnO₂:TiO₂/FPCFs, which is due to the synergetic effect of TiO₂ achieved in this study.

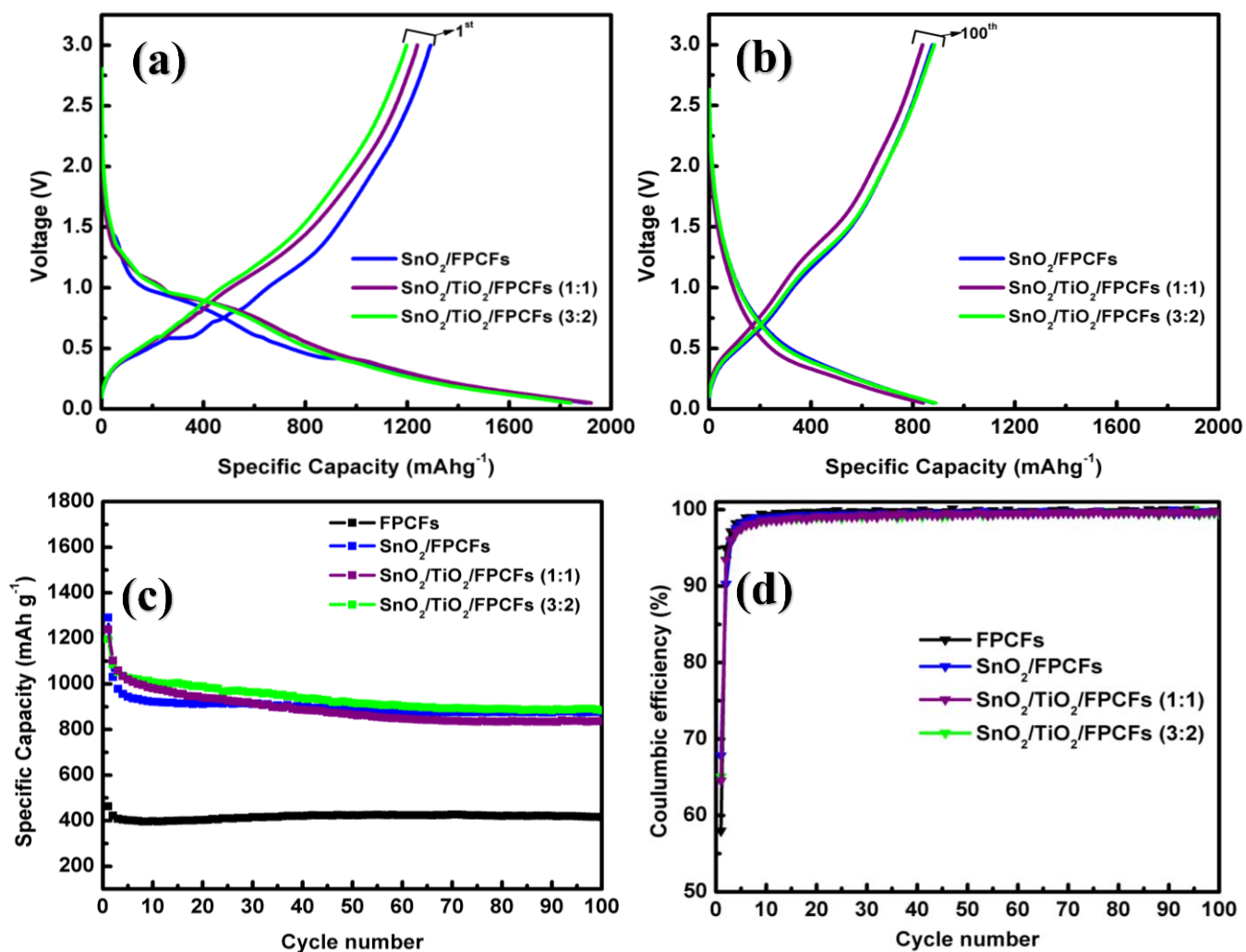


Figure 31. Charge/discharge curves of the SnO₂/FPCFs, (1:1) SnO₂:TiO₂/FPCFs, (3:2) SnO₂:TiO₂/FPCFs at the 1st (a) and 100th (b) as well as the charge capacity (c) and coulombic efficiency (d) after 100 cycles at a current density of 100 mA g⁻¹.

Furthermore, to gain more insight on the cycling performance of the ceramic/carbon composites, charge/discharge cycles were also carried at 200 mA g^{-1} for 100 cycles over a potential of 0.05-3.0V. As expected, it can be observed in Figure 32 (a, b) that the fibers coated with $\text{SnO}_2\text{:TiO}_2/\text{FPCFs}$ demonstrated better cycling stability when compared to that of the $\text{SnO}_2/\text{FPCFs}$, which is due to the addition of TiO_2 which reduced the capacity loss at the first 20 cycles. At the first cycle, the $\text{SnO}_2/\text{FPCFs}$ demonstrated a higher charge capacity of 636 mAh g^{-1} when compared to that of the (1:1) $\text{SnO}_2\text{:TiO}_2/\text{FPCFs}$ and (3:2) $\text{SnO}_2\text{:TiO}_2/\text{FPCFs}$ which delivered a charge capacity of 568, and 591 mAh g^{-1} , respectively. The lower capacity delivered by the (1:1) $\text{SnO}_2\text{:TiO}_2/\text{FPCFs}$ was caused by the addition of TiO_2 which hindered the overall lithium storage of the composite due to its low theoretical capacity. However, after 100 cycles, the (3:2) $\text{SnO}_2\text{:TiO}_2/\text{FPCFs}$ retained a larger capacity of 420 mAh g^{-1} while the SnO_2 and the (1:1) $\text{SnO}_2\text{:TiO}_2/\text{FPCFs}$ ratio only yielded a capacity of 369 and 370 mAh g^{-1} , respectively. The improved electrochemical performance of the (3:2) $\text{SnO}_2\text{:TiO}_2/\text{FPCFs}$ can once again be attributed to the contribution of TiO_2 which can mitigate the large volume expansion of SnO_2 during lithiation/delithiation, improving the capacity retention and also the overall cycling stability.

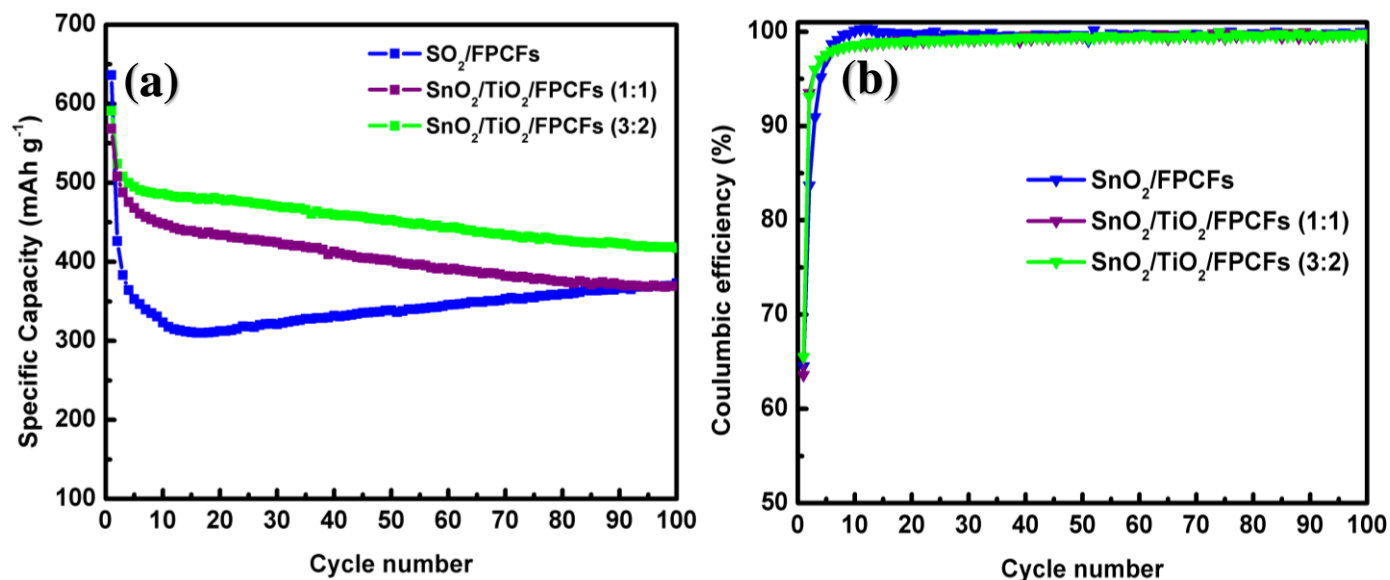


Figure 32. Charge profiles (a) and coulombic efficiency (b) of the SnO₂/FPCFs, (1:1) SnO₂:TiO₂/FPCFs, and (3:2) SnO₂:TiO₂/FPCFs ceramic/carbon composite fibers after 100 cycles at a current density of 200 mA g⁻¹.

To investigate the rate capability of the ceramic/carbon composites, charge/discharge experiments were performed at 50, 100, 200, 400, 500, and back at 50 mA g⁻¹ for 10 cycles. It can be seen in figure 33 that the fibers coated with (3:2) SnO₂:TiO₂ outperformed all the other composites. When the current density was increased to 500 mAh g⁻¹, the (3:2) SnO₂:TiO₂/FPCFs retained a capacity of 323 mAh g⁻¹ while the SnO₂/FPCFs and the pure FPCFs showed a capacity of 210 and 130 mAh g⁻¹, respectively. In contrast, the (1:1) SnO₂:TiO₂/FPCFs yielded the lowest capacity which was 39 mAh g⁻¹ which was caused by the excessive addition of TiO₂ that lowered the capacity of the overall composite. When the current density was brought back to 50 mA g⁻¹, the (3:2) SnO₂:TiO₂/FPCFs delivered a capacity of 908 mAh g⁻¹, while the pristine FPCFs yielded a capacity of 758, 727, and 424 mAh g⁻¹, at respectively. Most importantly, the (3:2) SnO₂:TiO₂/FPCFs demonstrated a 100% reversibility and the highest capacity achieved when compared to that of the SnO₂/FPCFs, (1:1) SnO₂:TiO₂/FPCFs which makes this composite a material of interest for use as an anode material in LIBs.

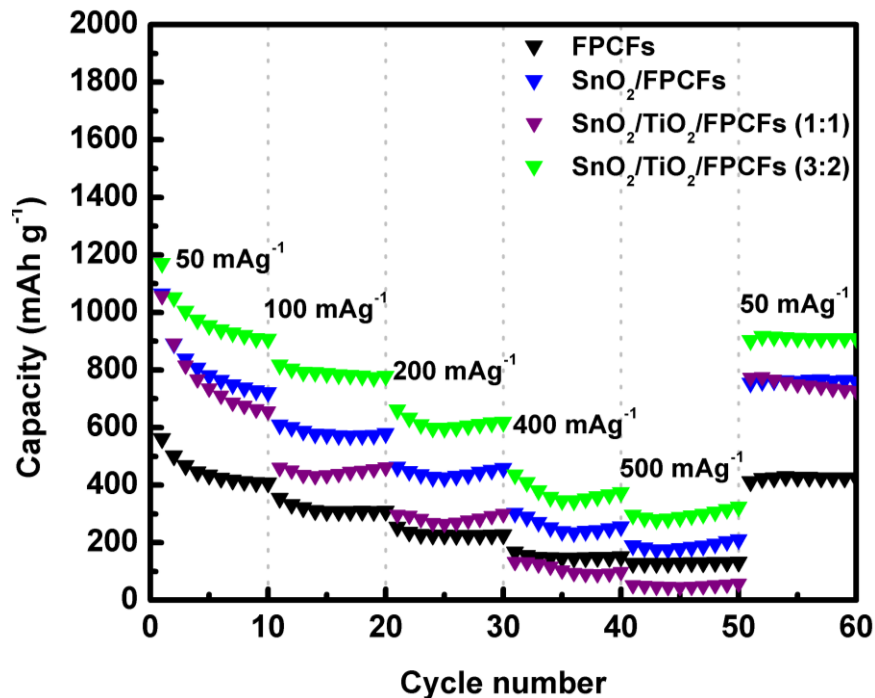


Figure 33. Rate performance of the $\text{SnO}_2/\text{FPCFs}$, (1:1) $\text{SnO}_2:\text{TiO}_2/\text{FPCFs}$, and (3:2) $\text{SnO}_2:\text{TiO}_2/\text{FPCFs}$ ceramic/carbon composite fibers at different current densities.

To further study and analyze the electrochemical properties and kinetics of the as-prepared anodes, electrochemical impedance spectroscopy (EIS) measurements were performed at an open circuit voltage and the results are shown in Figure 34. The Nyquist plots in Figure 34 (a) can be divided into two sections which are the semicircle located at the high-medium frequencies and the slope line in the low frequency range. The semicircle can be ascribed to the diffusion of Li-ions through the SEI layer and the charge transfer resistance at the electrode-electrolyte interface. Next, the slanted slope line at the low frequencies is assigned to the diffusion of Li ions through the active material. The EIS results were analyzed and fitted by the equivalent circuit illustrated in Figure 34 (b). In this circuit, R_s , R_{ct} , W , and CPE represent the electrolyte solution resistance, the charge transfer resistance, the Warburg impedance, and the phase-angle element that is equivalent to the double layer capacitance, respectively. Based on Nyquist plots shown in Figure 34 (a), the FPCFs, $\text{SnO}_2/\text{FPCFs}$, (1:1) $\text{SnO}_2:\text{TiO}_2/\text{FPCFs}$, and

(3:2) $\text{SnO}_2\text{:TiO}_2/\text{FPCFs}$, demonstrated an overall resistance of 500, 430, 570, and 370 Ω , respectively. The improved resistance of the (3:2) $\text{SnO}_2\text{:TiO}_2/\text{FPCFs}$ can be attributed to the heterojunction formed between Sn, SnO_2 and TiO_2 as well as the synergistic effect of the particles within the flexible porous matrix which resulted in improved Li transport and lower charge transfer resistance when compared to the other composite electrodes [33].

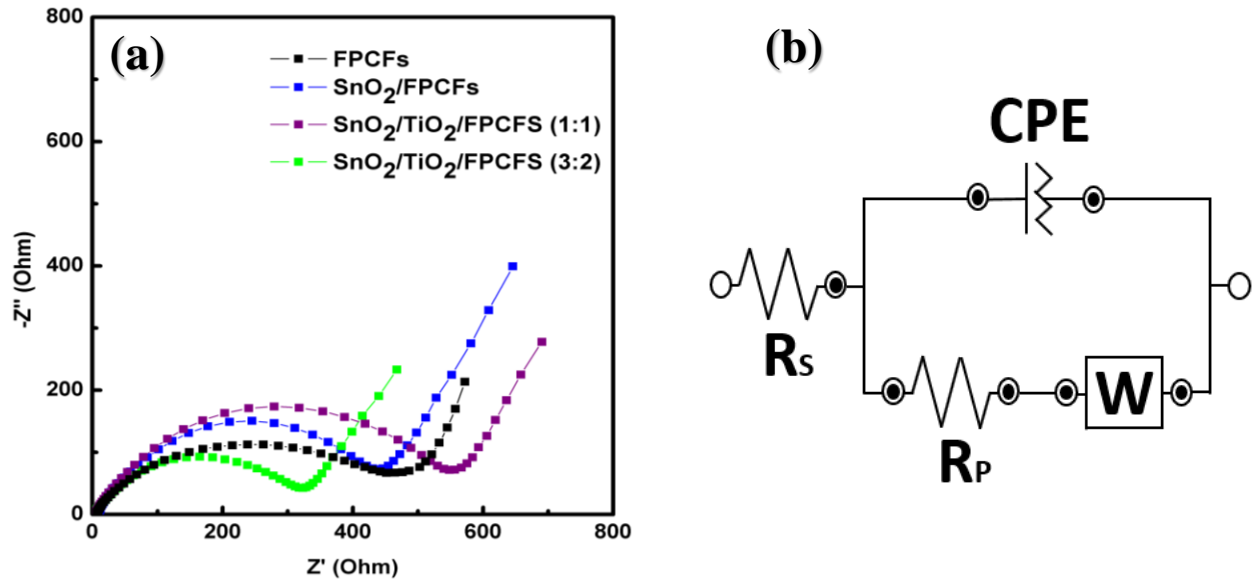


Figure 34. Nyquist impedance (a) of the $\text{SnO}_2/\text{FPCFs}$, (1:1) $\text{SnO}_2\text{:TiO}_2/\text{FPCFs}$, and (3:2) $\text{SnO}_2\text{:TiO}_2/\text{FPCFs}$ ceramic/carbon composite fibers before cycling and the equivalent circuit (b)

CHAPTER V

CONCLUSION

Short $\text{SnO}_2\text{:TiO}_2$ micro belt-fibers were successfully synthesized through safe, facile, and fast processing fiber production method. The short micro-belt fibers were synthesized using tin and titanium precursors mixed in ethanol/PVP, which was used in the centrifugal spinning process. The calcination of the precursor fibers in air at $700\text{ }^\circ\text{C}$ resulted in a short micro belt-fiber morphology with spherical particles on the surface which was observed by the SEM studies. Furthermore, the phases, stability, and elemental composition of $\text{SnO}_2\text{:TiO}_2$ were confirmed using EDS, XPS, and TGA analysis. The XRD patterns confirmed the presence of crystal structure of SnO_2 and the rutile phase of TiO_2 within the fibers. In addition, when used as an anode material in LIBs, the $\text{SnO}_2\text{:TiO}_2$ micro belt-fibers demonstrated initial irreversible capacity of 1200 mAh g^{-1} and reversible charge capacity of 820 mAh g^{-1} when tested at a current rate of 100 mA g^{-1} . However, due to the pulverization of the anode upon cycling, the reversible capacity decreased to 279 mAh g^{-1} after 70 cycles. Additionally, the SnO_2 and $\text{SnO}_2\text{:TiO}_2$ composite fibers were successfully coated onto centrifugally spun PAN/PMMA fibrous mats which yielded ceramic/carbon composite fibers after a subsequent heat treatment. The surface morphology and structure of the as-prepared composite fibers was investigated by SEM which confirmed that the particles were successfully attached to the surface of the carbon porous fibers. The presence, phases, and crystal structure of metallic Sn, SnO_2 as well as TiO_2

within the carbon composite fibers was confirmed by EDS, XPS and TGA, respectively. Moreover, when used as a binder-free anode in LIBs, the (3:2) $\text{SnO}_2\text{:TiO}_2/\text{FPCFs}$ delivered a high reversible capacity of 890 mAh g^{-1} after 100 cycles at 100 mA g^{-1} . More interestingly, when tested at a high current density of 200 mA g^{-1} , the composite-fiber anode delivered a capacity of 419 mAh g^{-1} after 100 cycles and coulombic efficiency of 99 % after the 2nd cycle up to the 100th cycle, indicating good cyclic stability and performance. In addition, when tested at different current densities, the (3:2) $\text{SnO}_2\text{:TiO}_2/\text{FPCFs}$ initially delivered a capacity of 1171 mAh g^{-1} at 50 mA g^{-1} and retained a capacity of 323 mAh g^{-1} at high current rate of 500 mA g^{-1} . After the current density was lowered back to 50 mA g^{-1} , the (3:2) $\text{SnO}_2\text{:TiO}_2/\text{FPCFs}$ delivered a capacity of 908 mAh g^{-1} , depicting great rate capabilities. The overall electrochemical performance demonstrated by the ceramic/carbon composite shows a great potential for use as anode in LIBs.

CHAPTER VI

FUTURE WORK

For future work it is important to improve the subsequent treatment of both the pure ceramic fibers and the ceramic/carbon fiber composites. This may help retain the structure of the SnO_2 and $\text{SnO}_2\text{:TiO}_2$ ceramic fibers when being coated onto the FPCFs. Moreover, by improving the subsequent heat treatment, the reduction of SnO_2 to metallic Sn can also be avoided. Furthermore, the percentage of pure ceramic fibers being coated onto the FPCFs can also be optimized to achieve better particle distribution after the heat treatment and enhance the electrochemical performance.

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BIOGRAPHICAL SKETCH

Gabriel Gonzalez was born in Mission, Texas in August 17, 1997 where he currently resides at 301 S Inspiration Rd, Mission, Texas, 78572. However, for the first 9 years of his life, Gabriel was raised in Reynosa and Rio Bravo, Tamaulipas, Mexico. At the age of 10, Gabriel's mother decided to move to the United States in the hopes of a better future. Gabriel's interest for math and science begun in the 5th grade when he was pronounced student of the year at his elementary. His science teacher at the time, Mr. Coronado, would always encourage him to believe in himself and aim for greatness. In 2012 Gabriel enrolled at Mission High School but due to personal issues transferred to Donna High School in 2014. It was there where his counselor and math teacher encouraged him to apply for a dual enrollment engineering academy (DEEA) with South Texas College (STC). In 2017 due to a tragic event, Gabriel transferred back to Mission High School where he graduated as the fifth ranking student of his class, an engineering associate's degree from STC, and a full ride to college. Gabriel completed his undergraduate studies in Mechanical Engineering at The University of Texas Rio Grande in December 2018 and his master's degree in Mechanical Engineering with specialization in Materials Science Engineering in May 2021. Gabriel can be contacted via e-mail at gabriel_gonzalez9094@outlook.com